

PROJETO DNIT

TED 680/2020

Parâmetros de desempenho de materiais asfálticos

Leni Leite

04 de junho de 2025



Objetivos

Indicadores de desempenho de ligantes aplicados a frio e a quente

- ☐ Aplicados a quente é a meta do TED 680/2020
- ☐ Aplicados a frio

-

Avaliação dos ligantes aplicados a quente

Visão da COPPE – escolha de parâmetros reológicos

- Distinção dos ligantes modificados e não modificados;
- Permitir escolha adequada de materiais - MeDiNa;
- Correlações dos resultados de ensaios de ligantes e de misturas asfálticas para escolha dos parâmetros de especificação de ligantes;
- Verificação do enquadramento dos resultados de análises dos ligante quanto às especificações americanas e quanto a proposta de especificação da Petrobras;
- Análise dos ligantes quanto a parâmetros reológicos relacionados a trincamento por fadiga e deformação permanente;

Materiais estudados

| Código | Tipo |
|--------|-------|
| A1 | 50/70 |
| A2 | 50/70 |
| A3 | 50/70 |
| A4 | 30/45 |
| A5 | 50/70 |
| A6 | 30/45 |
| A7 | 50/70 |
| A8 | 50/70 |
| A9 | 50/70 |
| A10 | 30/45 |
| A11 | 50/70 |
| A12 | 50/70 |

| Código | Tipo |
|--------|-------|
| B1 | AB-8 |
| B2 | AB-8 |
| B3 | AB-8 |
| B4 | AB-22 |
| B5 | AB-8 |
| B6 | AB-22 |
| B7 | AB-8 |
| B8 | AB-8 |
| B9 | AB-8 |

| Código | Tipo |
|--------|-------|
| C1 | 76-28 |
| C2 | 55/75 |
| C3 | 60/85 |
| C4 | 55/75 |
| C5 | HiMA |
| C6 | 65/90 |
| C7 | 60/85 |
| C8 | 55/75 |
| C9 | 60/85 |
| C10 | 55/75 |
| C11 | 60/85 |
| C12 | 60/85 |
| C13 | 65/90 |
| C14 | 60/85 |
| C15 | 60/85 |
| C16 | 60/85 |

3 tipos de agregados

30 misturas asfálticas

| Tipo | Quantidade |
|-------|------------|
| 30/45 | 3 |
| 50/70 | 9 |

| Tipo | Quantidade |
|-------|------------|
| AB-8 | 7 |
| AB-22 | 2 |

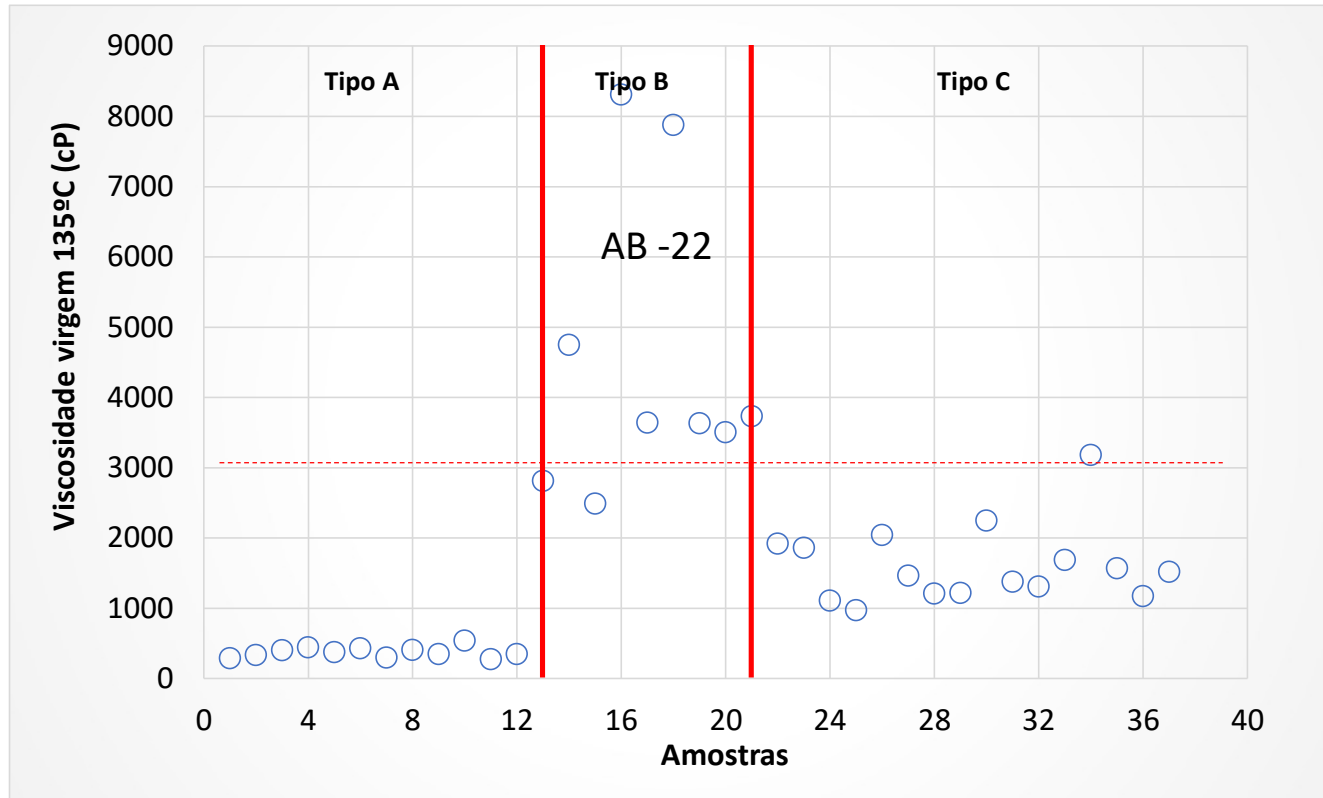
| Tipo | Quantidade |
|-------|------------|
| Russo | 1 |
| 55/75 | 4 |
| 60/85 | 8 |
| 65/90 | 2 |
| HiMa | 1 |

Avaliação dos ligantes aplicados a quente

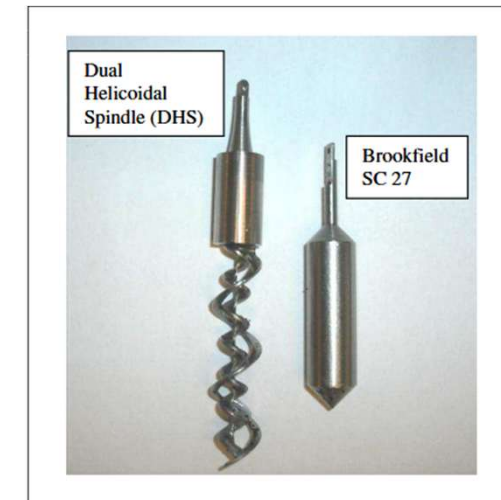
Avaliação dos ligantes asfálticos quanto ao enquadramento das especificações SUPERPAVE



Viscosidade Brookfield a 135°C, SP21, 20 RPM



| | | |
|----------------------------------------------|----|--------|
| Viscosidade rotacional a 135°C, SP21, 20 RPM | cP | ≤ 3000 |
|----------------------------------------------|----|--------|



AB necessita de ensaio apropriado

Lo Presti

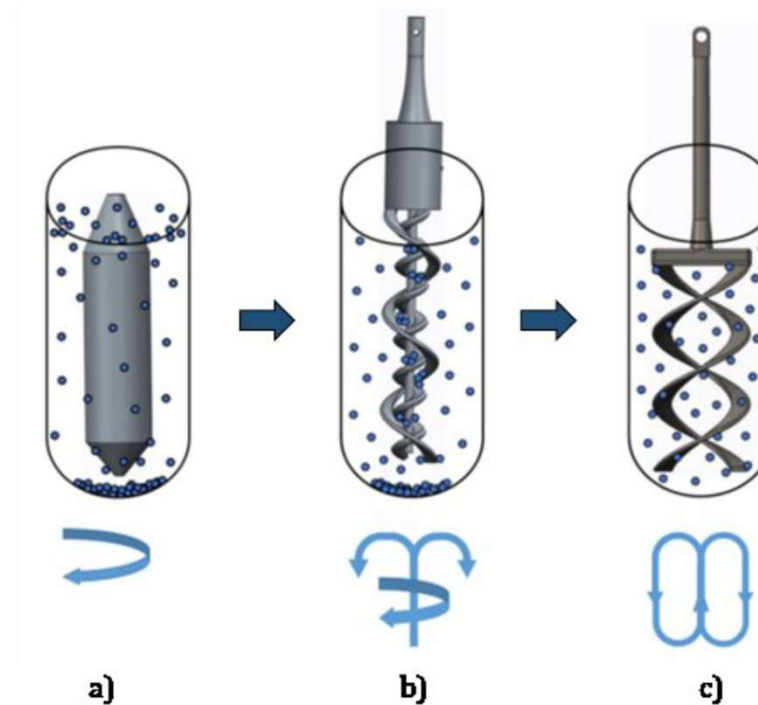
Are we correctly measuring the rotational viscosity of rubberized bituminous binder?

Conference Paper · October 2020

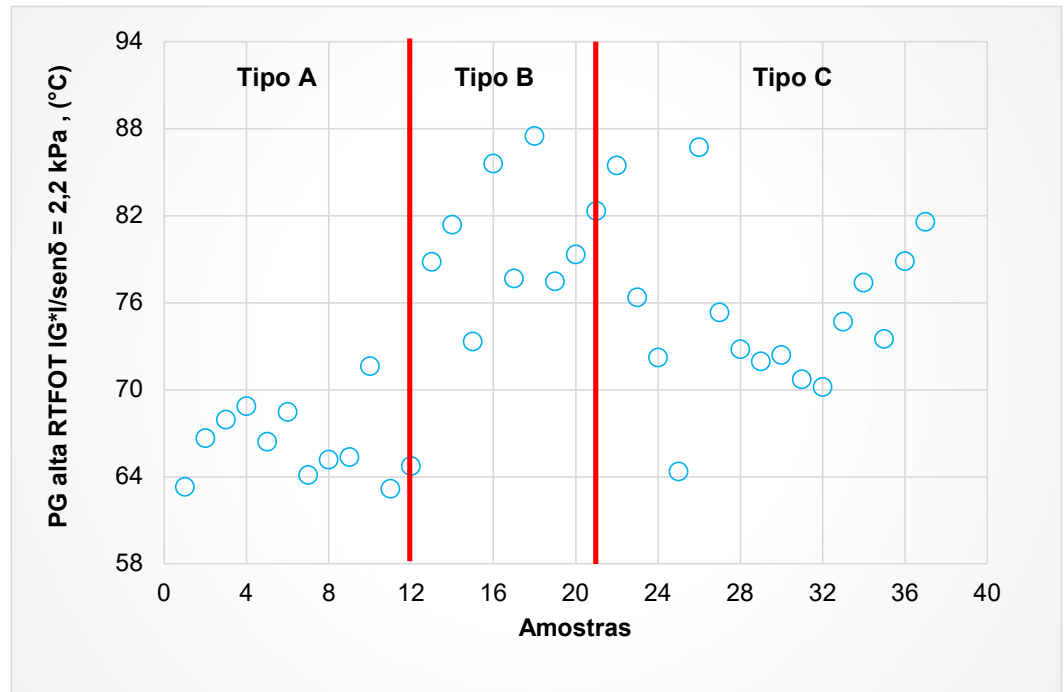
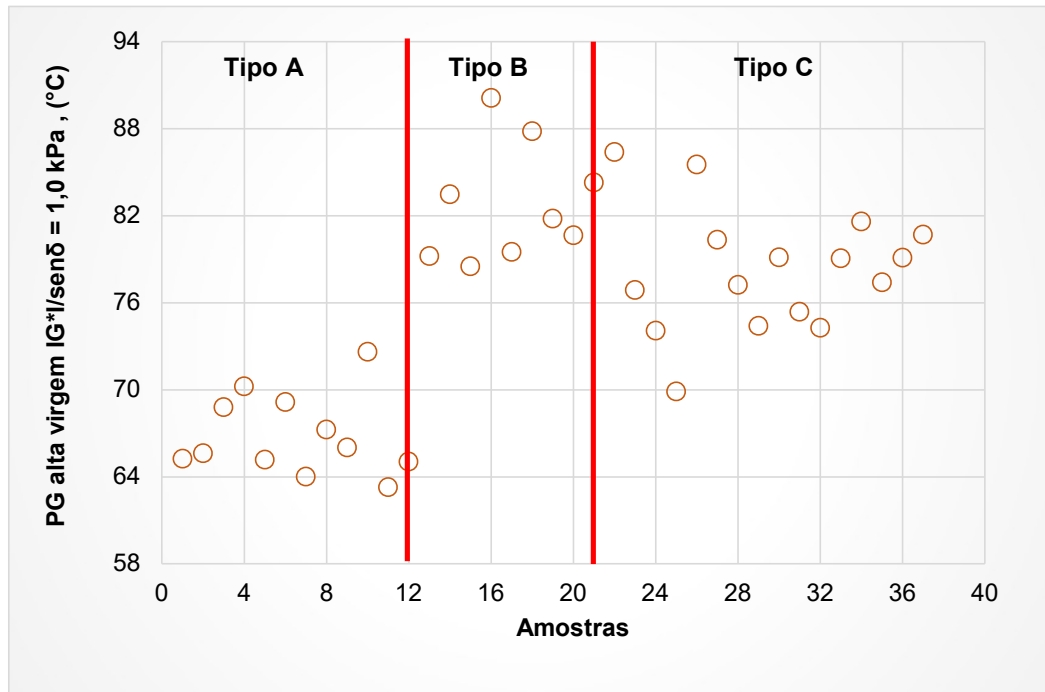


Distribuição das partículas de GTR dentro da câmara usando diferentes geometrias

- a) standard spindle Sc-27,
- b) dual helical impeller (DHI),
- c) dual helical ribbon (DHR).

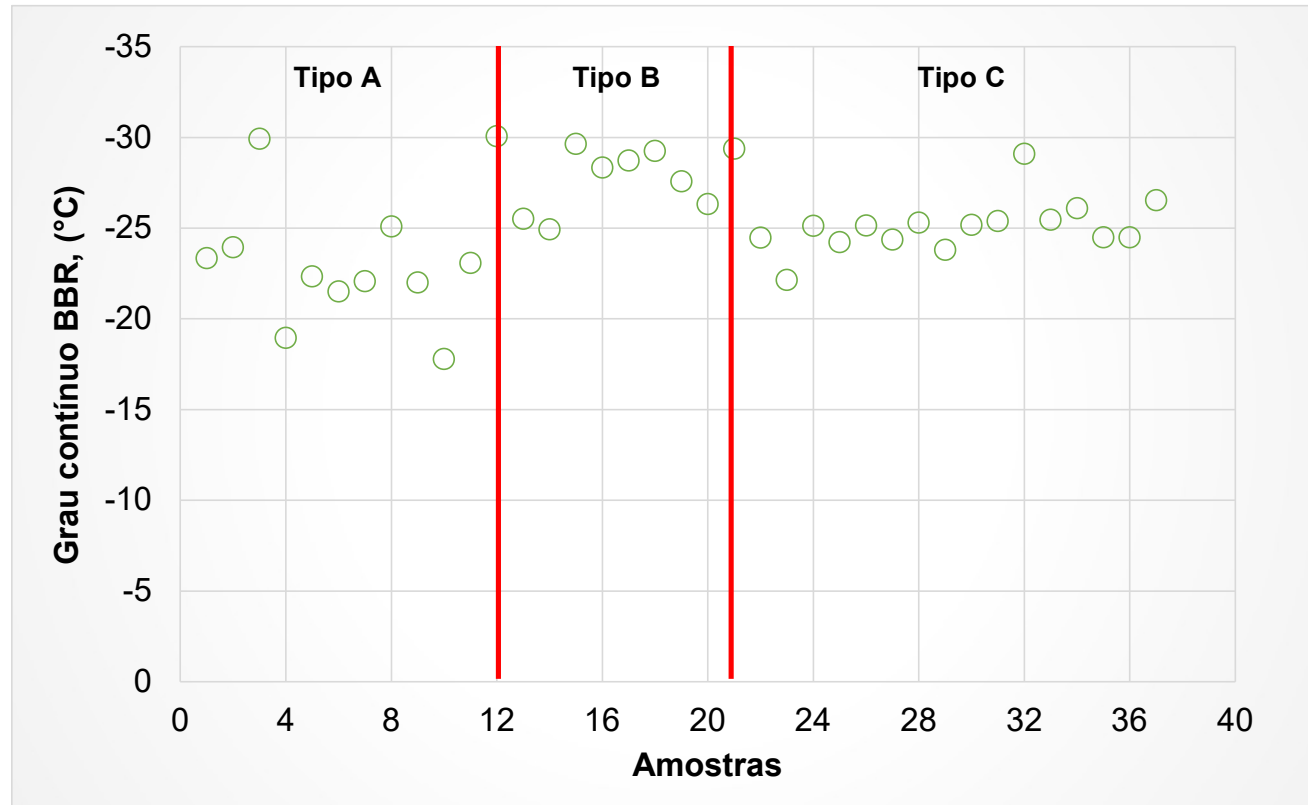


PG contínuo alta – virgem & RTFOT



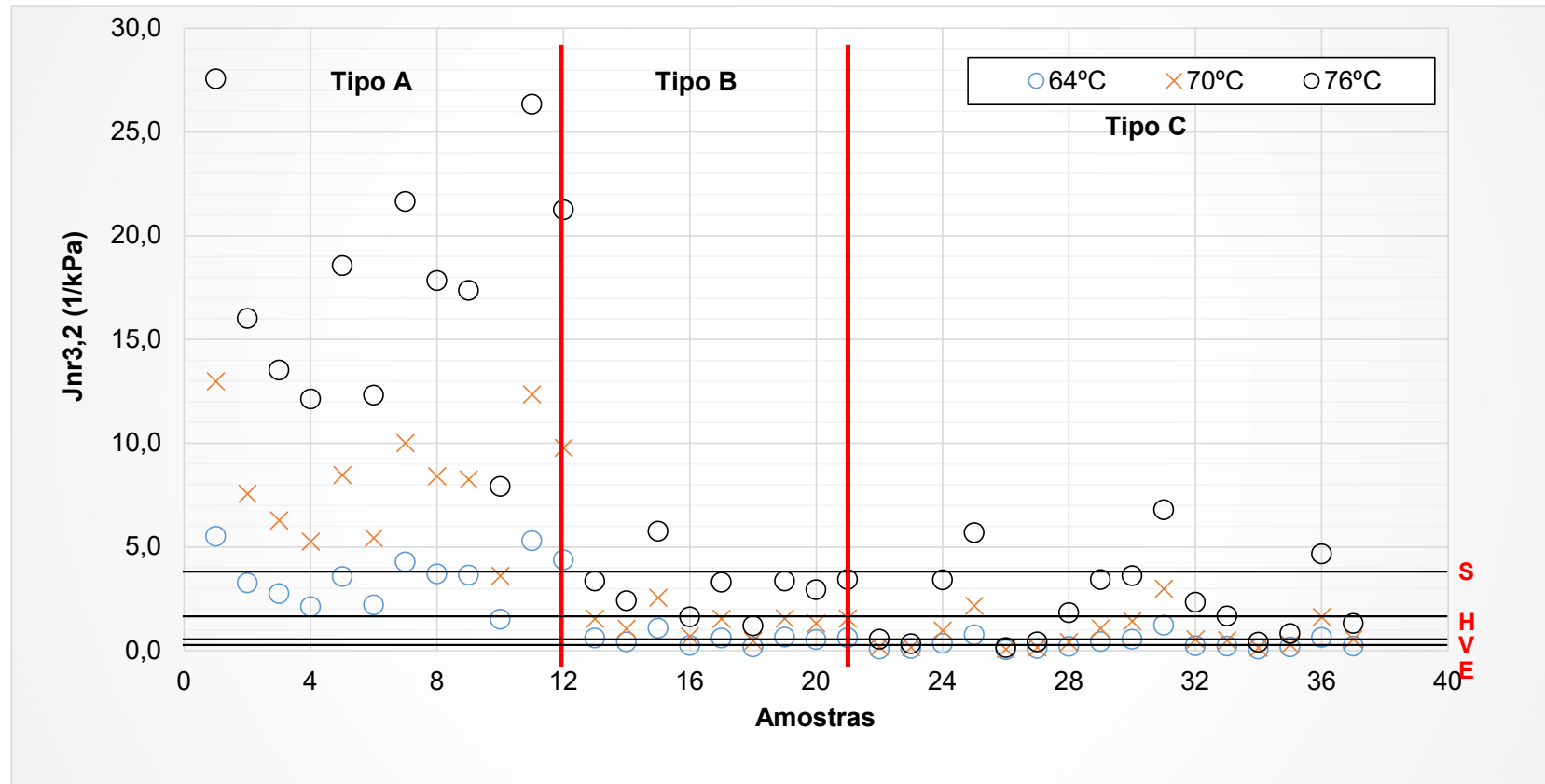
PG 58 a 88

PG baixa

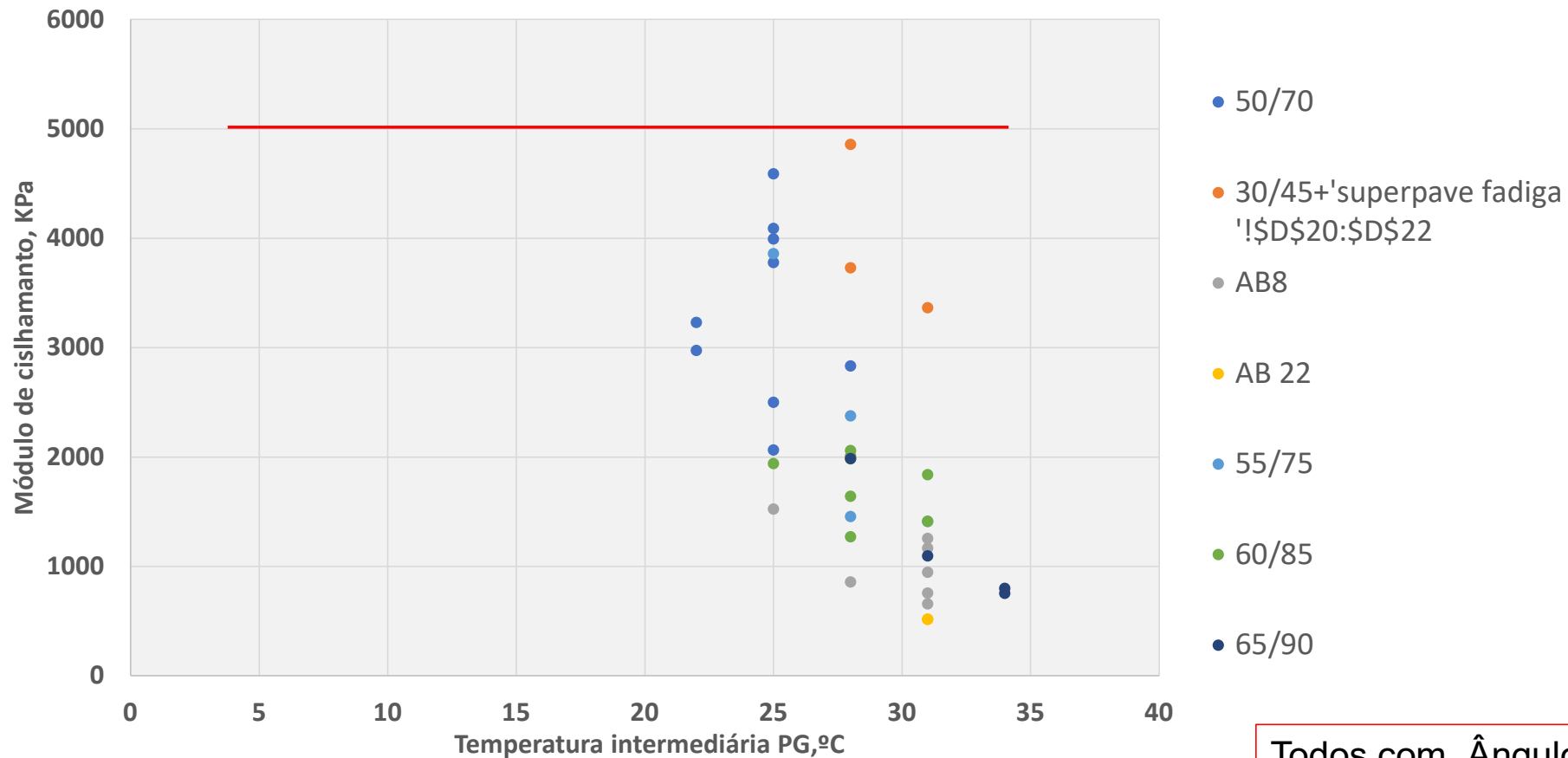


PG -28 a -16

MSCR – resistência a deformação permanente



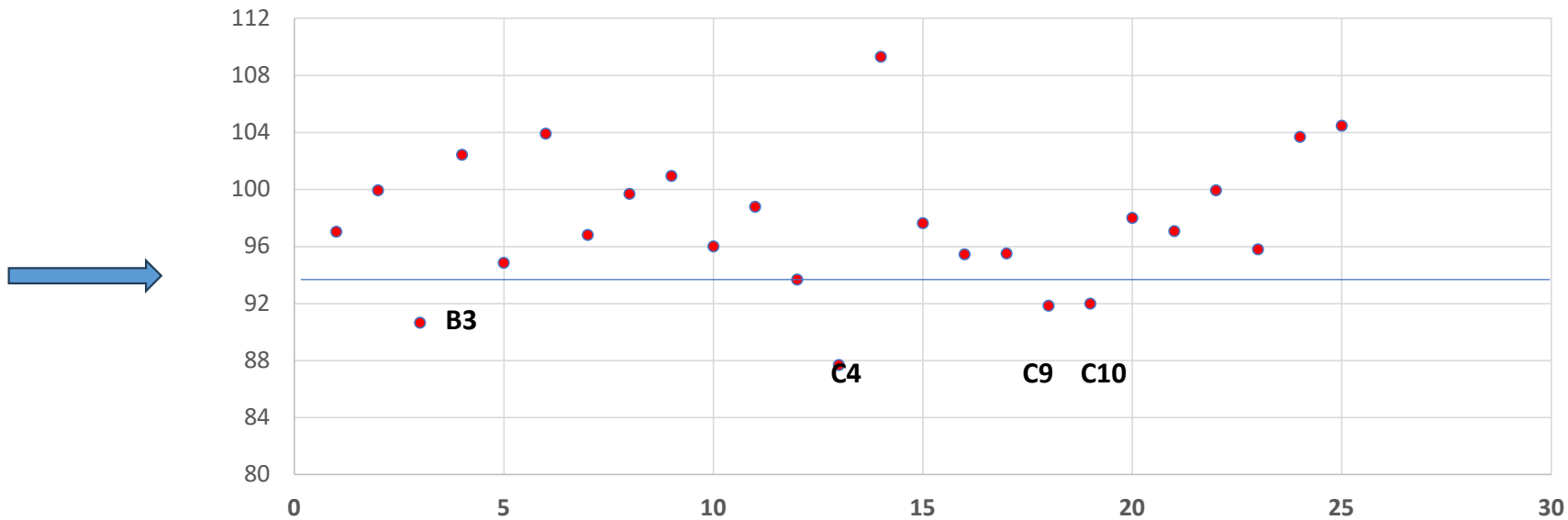
$G^* \cdot \sin \delta$ – resistência a trincas por fadiga



Todos com Ângulo de fase > 42

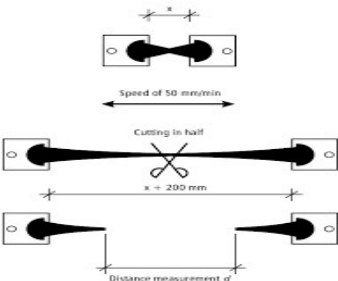
Faixa SUPERPAVE PG versus 92º (asfalto superior)

Faixa de PG AB e AMP

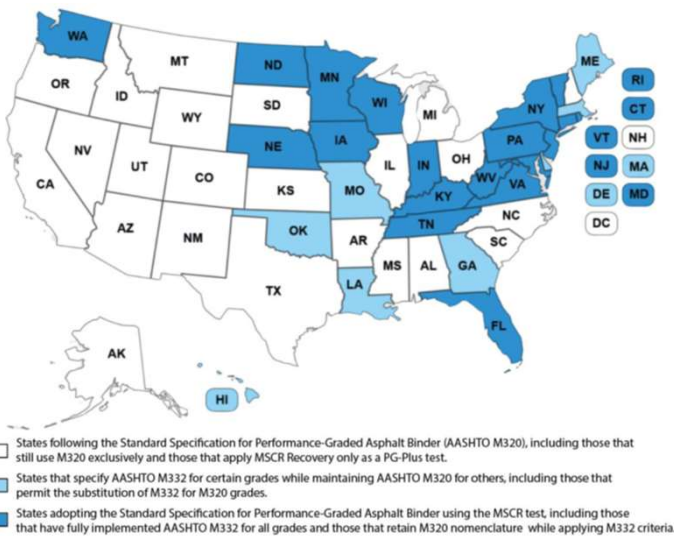
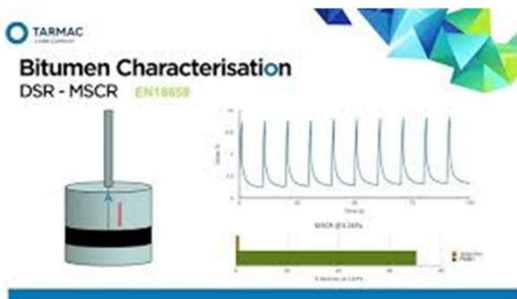


Ensaio plus com limites - DOT americanos

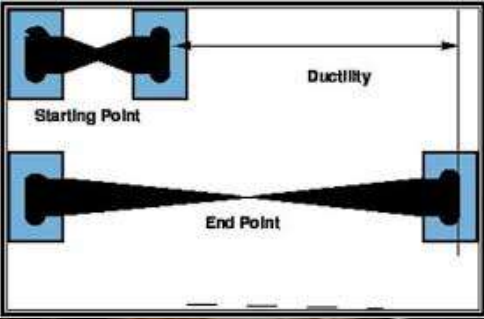
Retorno elástico (4 ou 25°C)



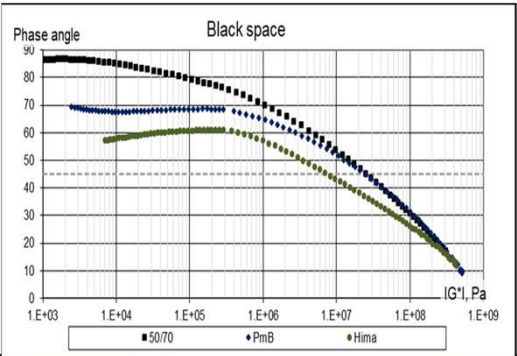
Recuperação elástica MSCR



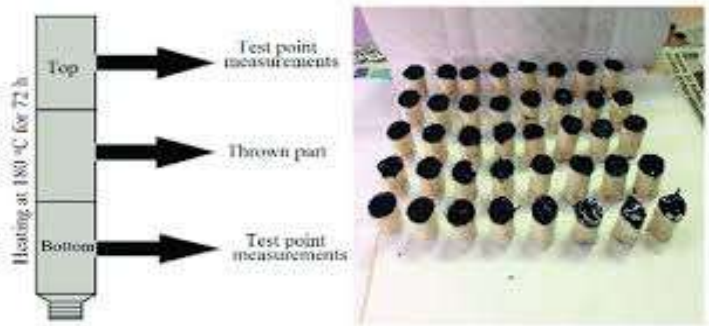
Ductilidade (4 ou 25°C)



Ângulo de fase PG alta



Estabilidade a estocagem



África do Sul

Considerações importantes

- Viscosidade a **165°C** alto cisalhamento;

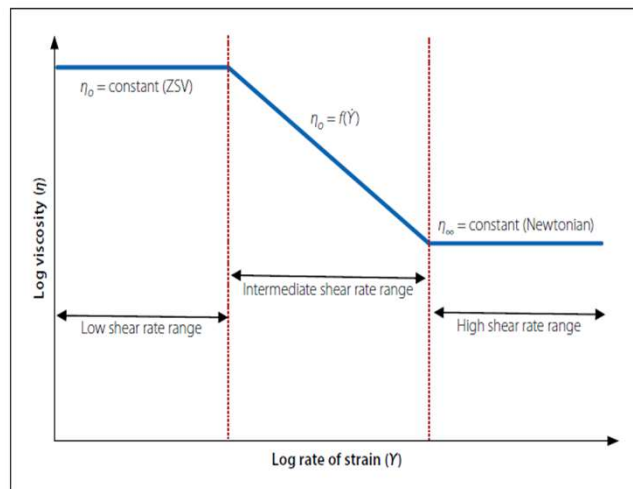


Figure 8 Schematic representation of viscosity ranges for bitumen

- Delta Tc;
- Estabilidade a estocagem a **180°C**;
- Parâmetro de envelhecimento **G^*_{env}/G^*_{vir}** a T intermediária (temperatura de 20 a 30°C) com índices semelhantes aos usados no passado para viscosidade a 60°C.

| Test Property | 58S-22 | 58H-22 | 58V-22 | 58E-22 | 64S-16 | 64H-16 | 64V-16 | 64E-16 | 70S-10 | 70H-10 | 70V-10 | 70E-10 | Test Method |
|---------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|----------------------|
| Max pavement design temperature (°C) (T_{max}) | 58 | 58 | 58 | 58 | 64 | 64 | 64 | 64 | 70 | 70 | 70 | 70 | |
| Minimum grading temperature (°C) (T_{min}) | -22 | -22 | -22 | -22 | -16 | -16 | -16 | -16 | -10 | -10 | -10 | -10 | |
| G^* and δ at $[(T_{max} + T_{min})/2+4]^{\circ}\text{C}$ | Compulsory report only – see detail description of report only item | | | | | | | | | | | | ASTM D7175 |
| $G^*\sin \delta$ @10rad/s (kPa) @ $T = T_{max}$ Report G^* and δ separately | Report only | | | | | | | | | | | | ASTM D7175 |
| Viscosity at 165°C (Pa.s) $\geq 30 \text{ sec}^{-1}$ | ≤ 0.9 | | | | | | | | | | | | ASTM D4402 |
| Storage stability at 180°C (% diff in G^* at T_{max}) | ≤ 15 | | | | | | | | | | | | ASTM D7175 |
| Flash Point (°C) | ≥ 230 | | | | | | | | | | | | ASTM D92b |
| After RTFO Aging | | | | | | | | | | | | | ASTM D2872 / TG1 MB3 |
| G^* and δ at $[(T_{max} + T_{min})/2+4]^{\circ}\text{C}$ | Compulsory report only – see detail description of report only item | | | | | | | | | | | | ASTM D7175 |
| Mass change (% m/m) | ≤ 0.3 | ≤ 1.0 | | ≤ 0.3 | ≤ 1.0 | | ≤ 0.3 | ≤ 1.0 | | | | | ASTM D2872 / TG1 MB3 |
| J_{NR} at T_{max} (kPa ⁻¹) | ≤ 4.5 | ≤ 2.0 | ≤ 1.0 | ≤ 0.5 | ≤ 4.5 | ≤ 2.0 | ≤ 1.0 | ≤ 0.5 | ≤ 4.5 | ≤ 2.0 | ≤ 1.0 | ≤ 0.5 | ASTM D7405 |
| Ageing ratio [$G^*_{RTFO}/G^*_{Original}$] | ≤ 3.0 | | | | | | | | | | | | ASTM D7175 |
| After RTFO plus PAV Aging | | | | | | | | | | | | | ASTM D6521 |
| G^* and δ at $[(T_{max} + T_{min})/2+4]^{\circ}\text{C}$ | Compulsory report only – see detail description of report only item | | | | | | | | | | | | ASTM D7175 |
| Maximum creep stiffness tested at temperature ($T_{min} + 10^{\circ}\text{C}$) , MPa, [S (60s) ≤ 300 MPa] | -12°C | | | | -6°C | | | | 0°C | | | | ASTM D6648 |
| Minimum m-value tested at temperature ($T_{min} + 10^{\circ}\text{C}$) , [m (60s) ≥ 0.300] | -12°C | | | | -6°C | | | | 0°C | | | | |
| ΔT_c (°C) = $T_{CS} - T_{CM}$ | ≥ -5 | | | | | | | | | | | | ASTM D7643 |
| Ageing ratio [$G^*_{PAV}/G^*_{Original}$] | ≤ 6.0 | | | | | | | | | | | | ASTM D7175 |

Conclusões – Superpave

O que pode ser melhorado

- África do Sul emprega viscosidade a altas taxas de cisalhamento e alta temperatura para AMP;
- Necessidade de incluir ensaio de envelhecimento (Tint ou T alta) ?
- Inclusão de ensaio de estabilidade a estocagem;
- Incluir ângulo de fase para distinção de modificados dos não modificados;
- Inclusão de ensaios empíricos (DOT) ?
- AB necessita de desenvolvimento de ensaio de viscosidade com spindle helicoidal ?;

Enquadramento das amostras

- Superpave diferencia ligantes no MSCR e no PG de alta temperatura, mas não diferencia na resistência à fadiga;
- Alguns ligantes AMP não são vistos como modificados, segundo a faixa de PG 92;

Avaliação dos ligantes asfálticos quanto ao enquadramento das especificações propostas pela Petrobras

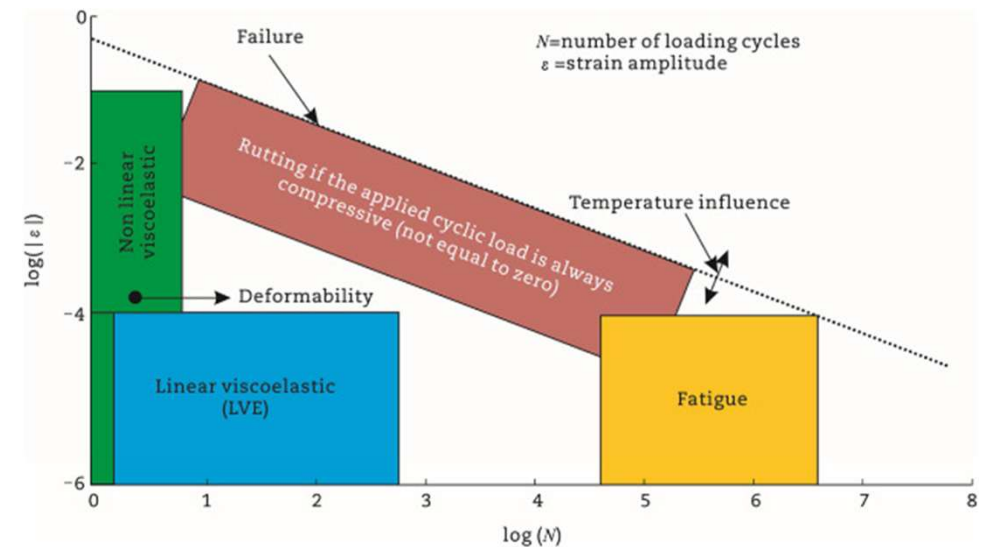


Proposta Petrobras

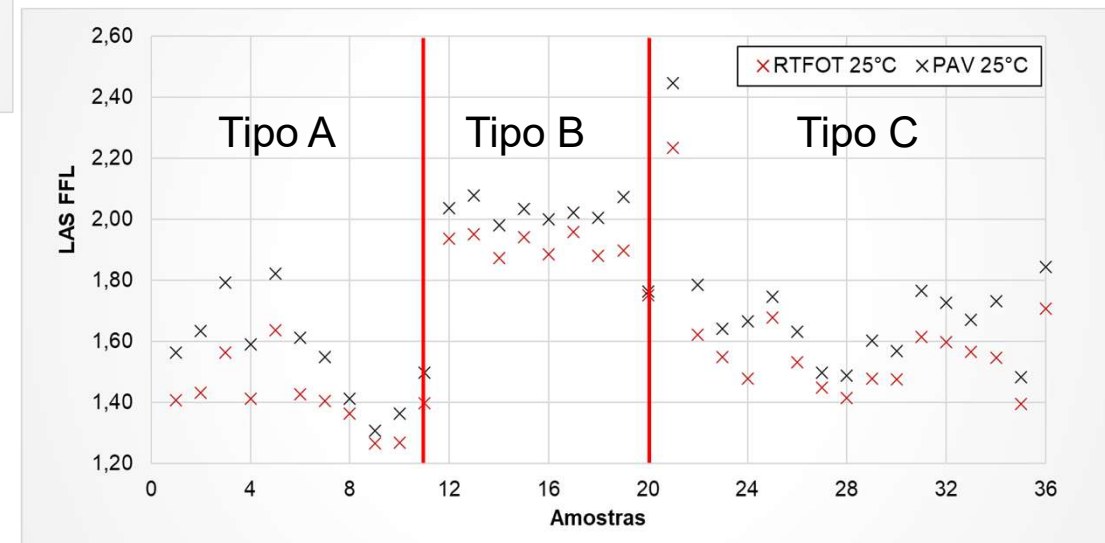
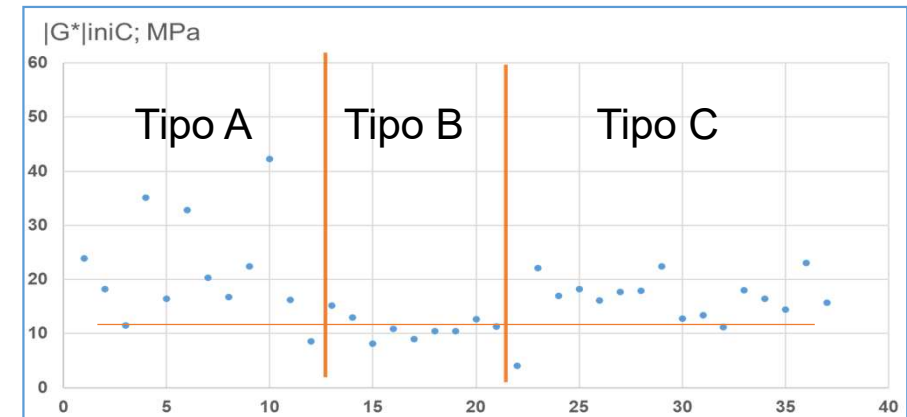
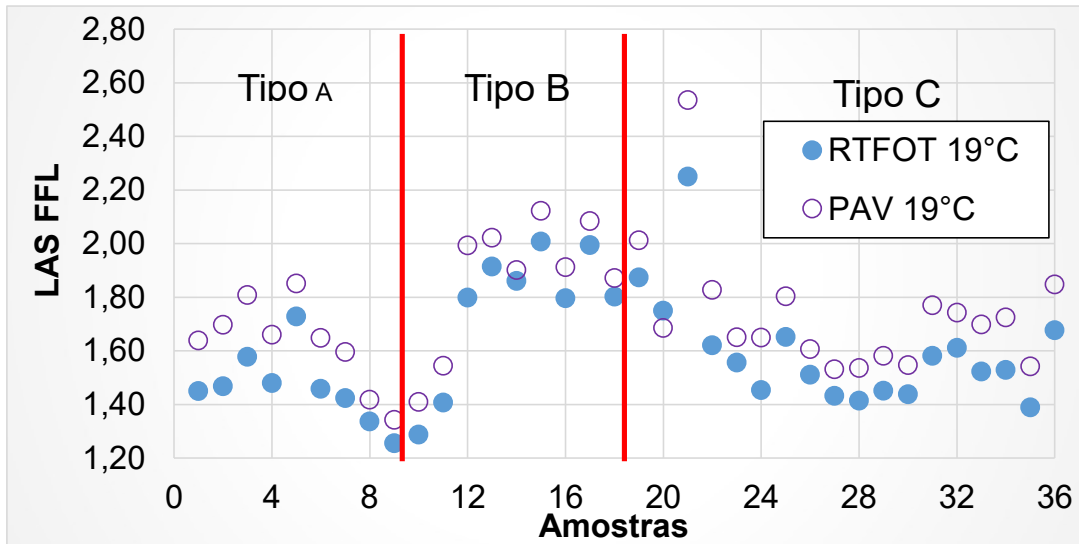
| Característica | Unidade | Limites | | | |
|-----------------------------------------------|---------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------|-------------------------------------------|-------------------------------------------|
| | | CAP 5 | CAP 10 | CAP 25 | CAP 40 |
| | | Ligante virgem | | | |
| $ G^* /\text{sen}(\delta)$ a 64°C e 1,59 Hz | kPa | $0,5 \leq G^* /\text{sen}(\delta) < 1,0$ | $1,0 \leq G^* /\text{sen}(\delta) < 2,5$ | $2,5 \leq G^* /\text{sen}(\delta) < 4,0$ | $4,0 \leq G^* /\text{sen}(\delta) < 6,0$ |
| Viscosidade rotacional a 135°C, SP21, 20 RPM | cP | ≤ 3000 | | | |
| Viscosidade rotacional a 150°C, SP21, 50 RPM | cP | ≤ 2000 | | | |
| Viscosidade rotacional a 177°C, SP21, 100 RPM | cP | ≤ 1000 | | | |
| Ponto de fulgor | °C | ≥ 235 | | | |
| Solubilidade em tricloroetileno | % massa | $\geq 99,5$ (apenas para ligantes não modificados) | | | |
| Ensaio de separação de fases | $R_{\text{topo/fundo}}^A$ | $0,7 \leq R_{\text{topo/fundo}} \leq 1,4$ (apenas para ligantes modificados) | | | |
| | | Ligante após RTFOT | | | |
| MSCR - J_{nr3200} a 64°C | 1/kPa | $\leq 9,25$ | $\leq 4,80$ | $\leq 2,50$ | $\leq 1,25$ |
| MSCR - $\% \gamma_{rec}$ a 64°C | % | $\begin{matrix} \text{Se } \% \gamma_{rec} \text{ a } 64^\circ\text{C} \geq 29,371 \times [J_{nr3200} \text{ a } 64^\circ\text{C}]^{-0,2633} - E \\ \text{Se } \% \gamma_{rec} \text{ a } 64^\circ\text{C} < 29,371 \times [J_{nr3200} \text{ a } 64^\circ\text{C}]^{-0,2633} - M \\ \text{(apenas para ligantes modificados)} \end{matrix}$ | | | |
| LAS – FFL_{PSE} a 19°C | log número de ciclos | $\geq 1,31^B$ | $\geq 1,22$ | | |
| LAS – $ G^* _{ini}^C$ a 19°C | MPa | $\leq 25,00$ | $\leq 40,00$ | $\leq 55,00$ | $\leq 75,00$ |
| Variação de massa | % massa | $\leq 1,00$ | | | |
| | | Classificação / denominação por desempenho | | | |
| Ligantes convencionais (não modificados) | | CAP 5-D-F | CAP 10-D-F | CAP 25-D-F | CAP 40-D-F |
| Ligantes modificados | | CAP 5-D-F-M | CAP 10-D-F-M | CAP 25-D-F-M | CAP 40-D-F-M |
| | | Sendo: D = Classe de deformação permanente (tabela IX) F = Classe de fadiga (tabela VIII) M = Designação utilizada quando o ligante tiver qualquer tipo de modificação: E ou M conforme $\% \gamma_{rec}$ a 64°C | | | |

Vantagens do Ensaio LAS

- Ser realizado fora da zona LVE, onde ocorre o dano;
- Correlação com ensaios de misturas asfálticas segundo experiencia brasileira ;
- Ensaio simples e rápido
- NCHRP - R e GRP (2022) são parâmetros LVE, sendo que R se correlaciona com LAS – FFL (PSE);



LAS / RTFOT & PAV



LAS, MSCR e R%

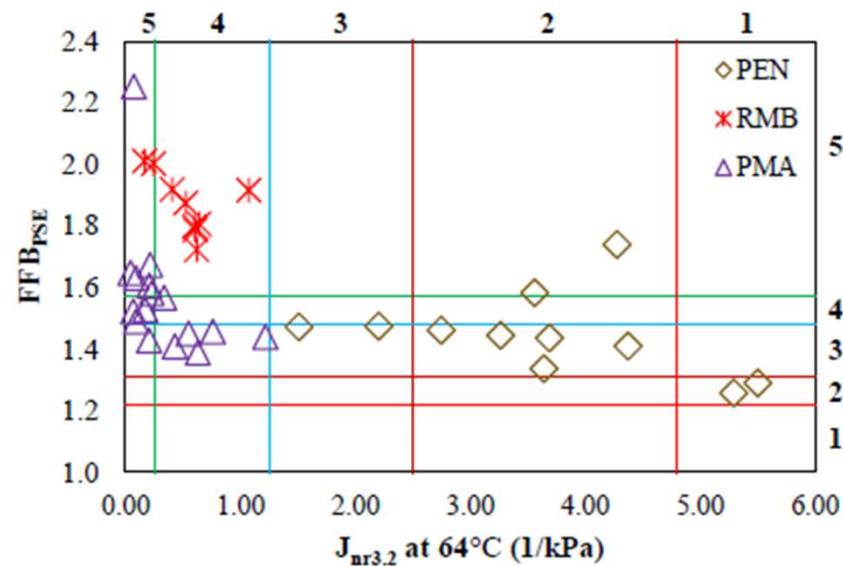
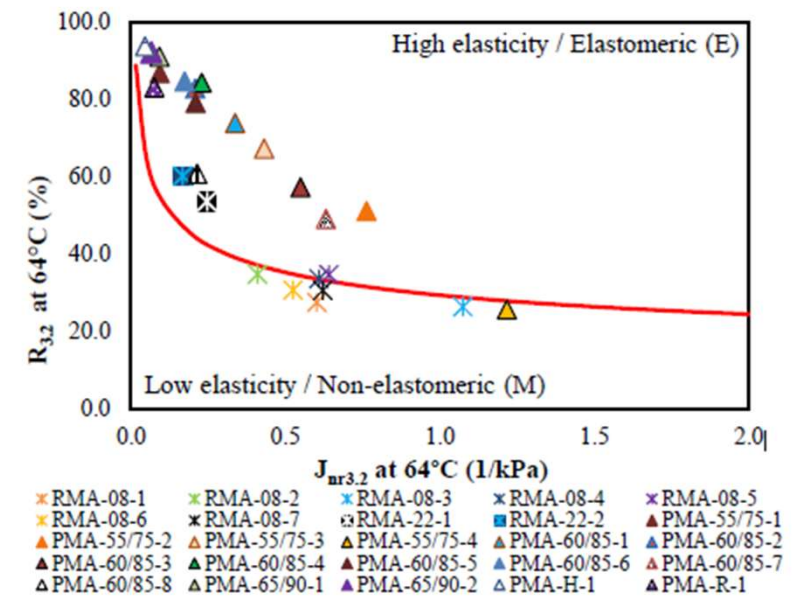


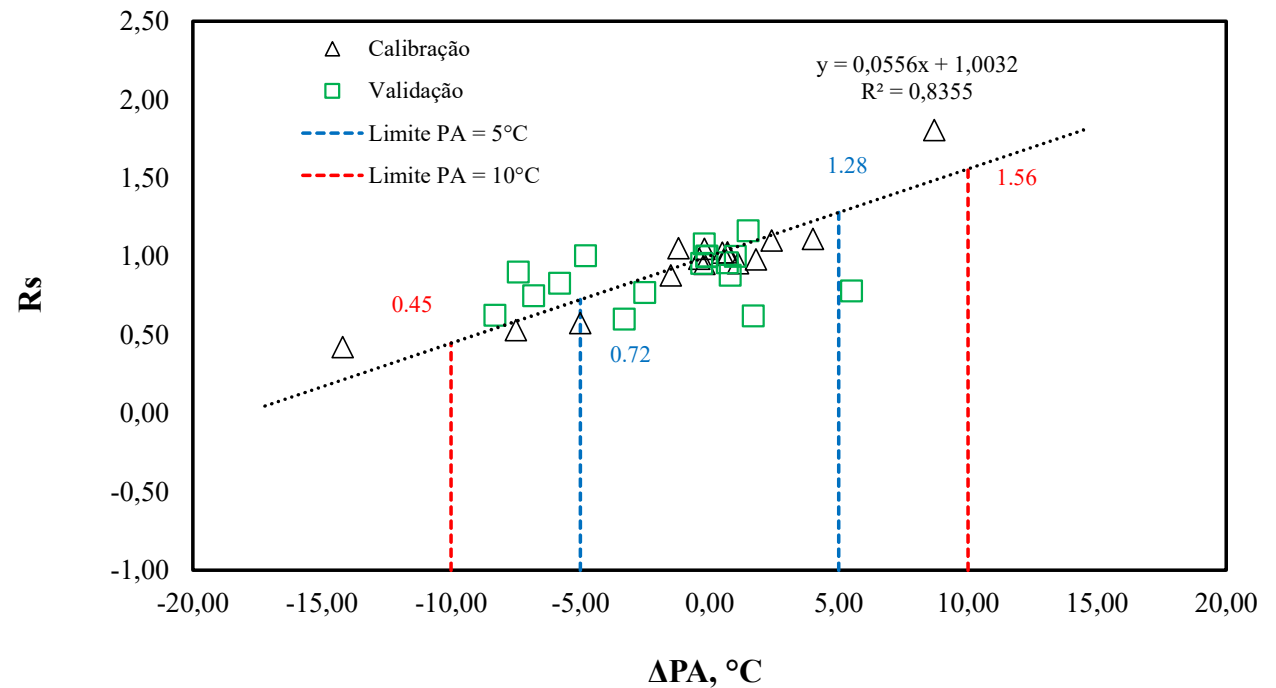
Figure 4.10 - Performance classification of asphalt binders based on Petrobras 2022 specification proposal for FFB_{PSE} at 19°C and $J_{nr3.2}$ at 64°C



Estabilidade a estocagem

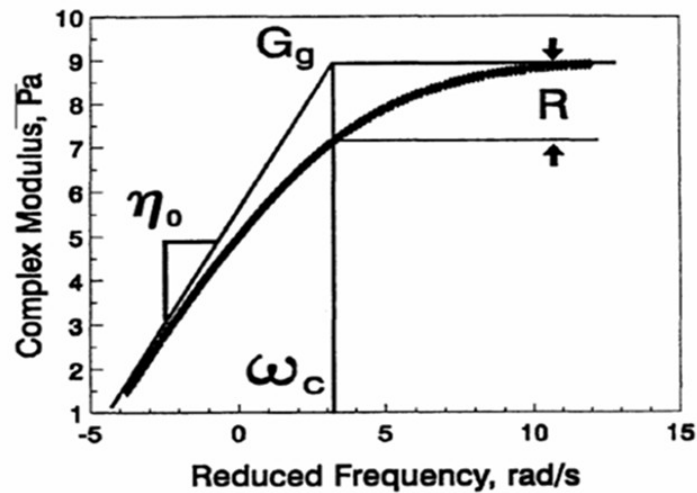
- R_s para asfaltos polímeros seriam de 0,72 e 1,28
- Literatura (0,80-1,20)
- Proposta Petrobras de 0,7 a 1,4.

Asfalto borracha entre 0,4 e 1,6

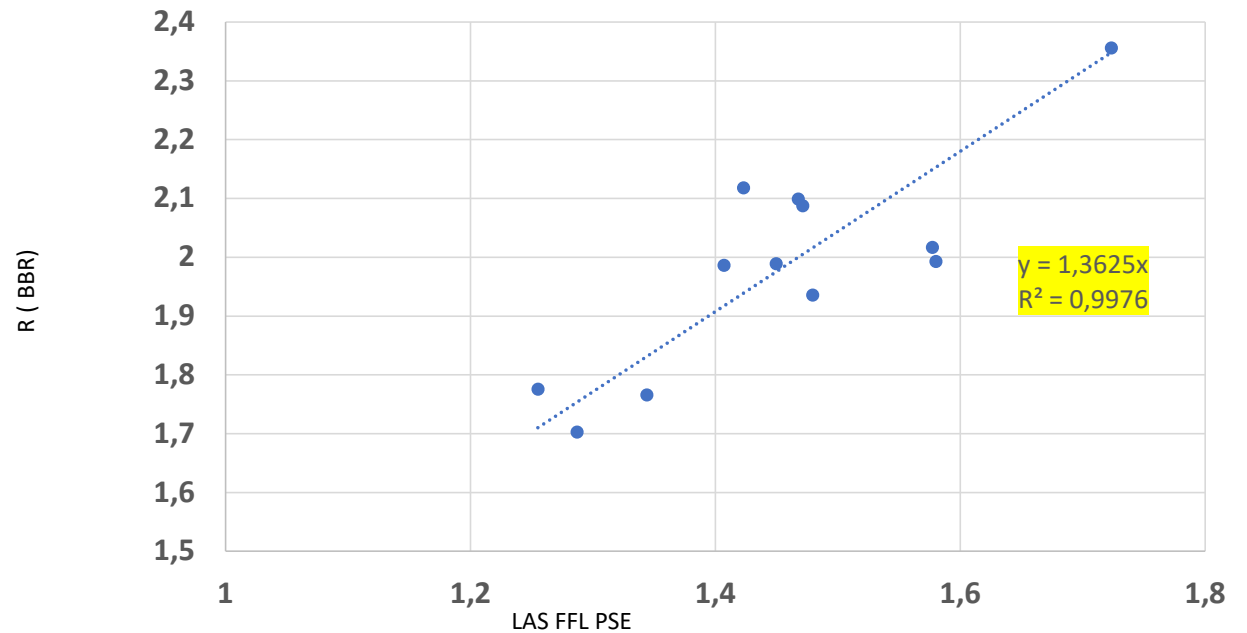


$$R_s = \frac{(|G^*|/s \text{ en} \delta)_t}{(|G^*|/s \text{ en} \delta)_b} \quad 64^\circ C$$

Correlações de índices de trincamento de CAP – LAS

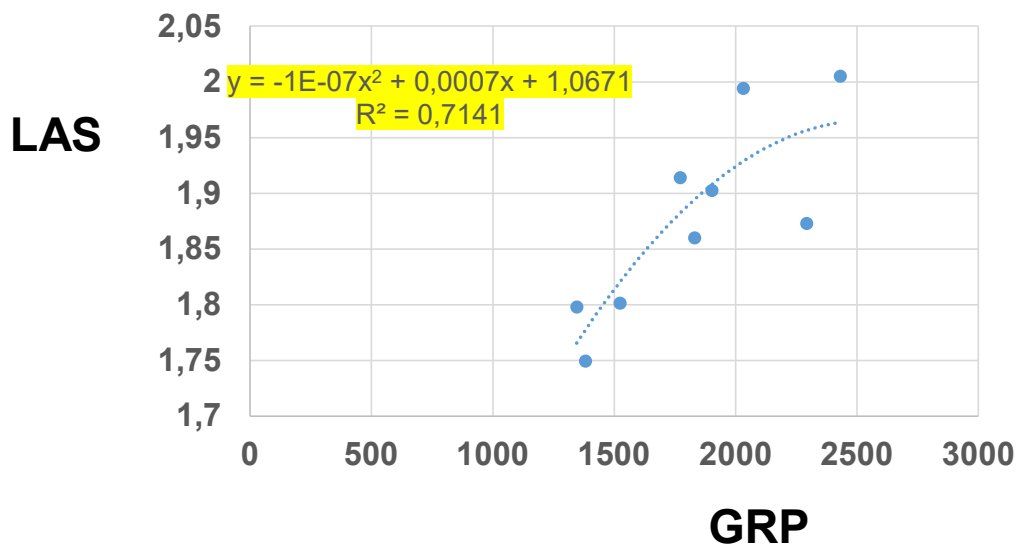


R (BBR) x LAS

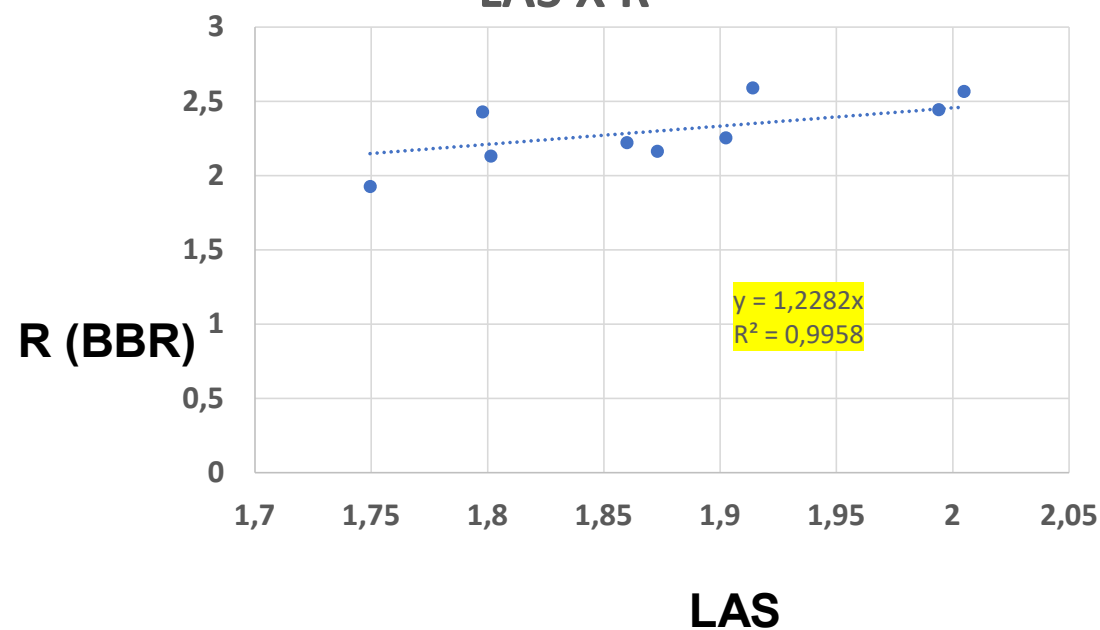


Correlações de índices de trincamento de AB – LAS

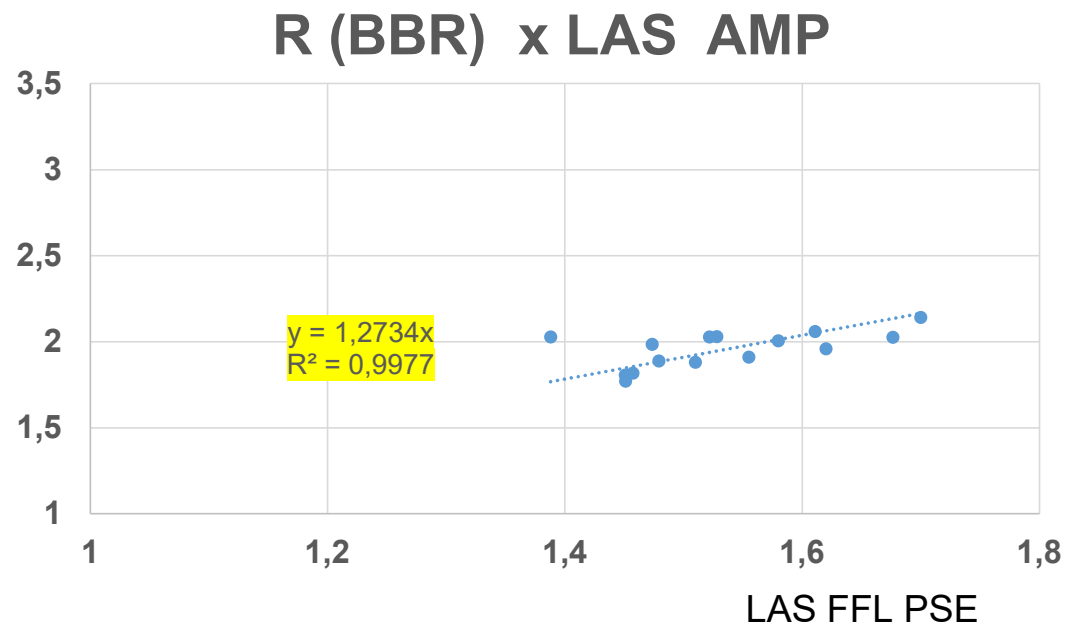
LAS x GRP



LAS X R



Correlações de índices de trincamento de AMP – LAS



Sem o AMP russo, apenas amostras ABEDA

Classificação proposta Petrobras

| | | DEF PERM | FADIGA |
|-----|-------|----------|--------|
| A1 | 50/70 | 1 | 3 |
| A2 | 50/70 | 2 | 3 |
| A3 | 50/70 | 2 | 5 |
| A4 | 30/45 | 3 | 3 |
| A5 | 50/70 | 2 | 5 |
| A6 | 30/45 | 3 | 3 |
| A7 | 50/70 | 2 | 3 |
| A8 | 50/70 | 2 | 3 |
| A9 | 50/70 | 2 | 2 |
| A10 | 30/45 | 3 | 2 |
| A11 | 50/70 | 1 | 3 |
| A12 | 50/70 | 2 | 5 |

CAP

Nenhum com desempenho XX
4-4 nem XX 5-5, classe 3 para
baixo

Classificação proposta Petrobras

| | | DEF PERM | FADIGA |
|----|-------|----------|--------|
| B1 | AB-8 | 4 | 5 |
| B2 | AB-8 | 4 | 5 |
| B3 | AB-8 | 4 | 5 |
| B4 | AB-22 | 5 | 5 |
| B5 | AB-8 | 4 | 5 |
| B6 | AB-22 | 5 | 5 |
| B7 | AB-8 | 4 | 5 |
| B8 | AB-8 | 4 | 5 |
| B9 | AB-8 | 4 | 5 |

AB

todos com desempenho entre XX 4-4 e XX 5-5

| | | DEF PERM | FADIGA |
|-----|-------|----------|--------|
| C1 | 76-28 | 5 | 5 |
| C2 | 55/75 | 5 | 5 |
| C3 | 60/85 | 4 | 4 |
| C4 | 55/75 | 4 | 3 |
| C5 | HiMA | 5 | 5 |
| C6 | 65/90 | 5 | 4 |
| C7 | 60/85 | 5 | 3 |
| C8 | 55/75 | 4 | 3 |
| C9 | 60/85 | 4 | 3 |
| C10 | 55/75 | 4 | 3 |
| C11 | 60/85 | 5 | 5 |
| C12 | 60/85 | 5 | 5 |
| C13 | 65/90 | 5 | 4 |
| C14 | 60/85 | 5 | 4 |
| C15 | 60/85 | 4 | 3 |
| C16 | 60/85 | 5 | 5 |

AMP

A maioria com desempenho entre XX 4-4 e XX 5-5, apenas 6 amostras com 3 na resistência a fadiga

Conclusões - Proposta Petrobras

- Há diferenciação de asfaltos modificados e não modificados por meio do FFL-PSE
- Não tem parâmetro de envelhecimento;
- Diferencia asfalto elastomérico por meio da recuperação elástica;
- Inclui estabilidade à estocagem;
- Segundo a especificação, CAP podem ser classe 1, ou 2, ou 3, enquanto AB podem ser classe 4, ou 5 e AMP podem ser classe 3, ou 4 ou 5;
- Também foi verificado que determinados AMP tem desempenho semelhante ao CAP quanto a fadiga.

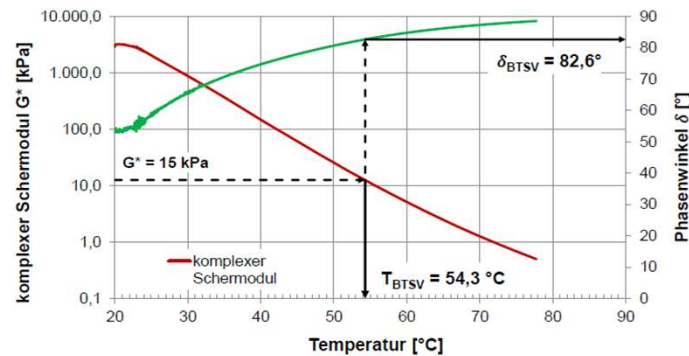
Avaliação dos ligantes asfálticos quanto aos índices reológicos

Alemanha

Test parameters

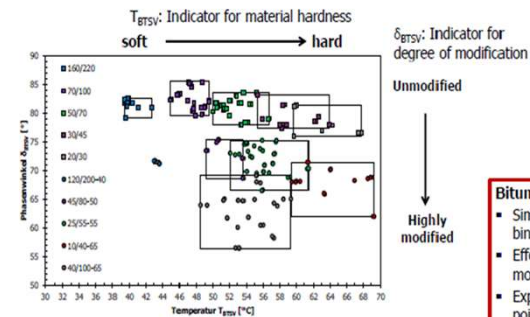
Binder-Fast-Characterization-Test (BTSV)

- Test geometry: 25 mm parallel-plate with a gap of 1 mm
- Test temperature: Starting temperature 20 °C, temperature rate 1.2 K/min
- Frequency: 1.59 Hz
- Shear stress: 500 Pa (oscillation)
- Characteristic values: Temperature T_{BTSV} at $G^* = 15 \text{ kPa}$ and associated phase angle δ_{BTSV}
- Test time including pre-tempering: 1.5 h



BTSV – Binder Fast Characterization Test

Binder characterization

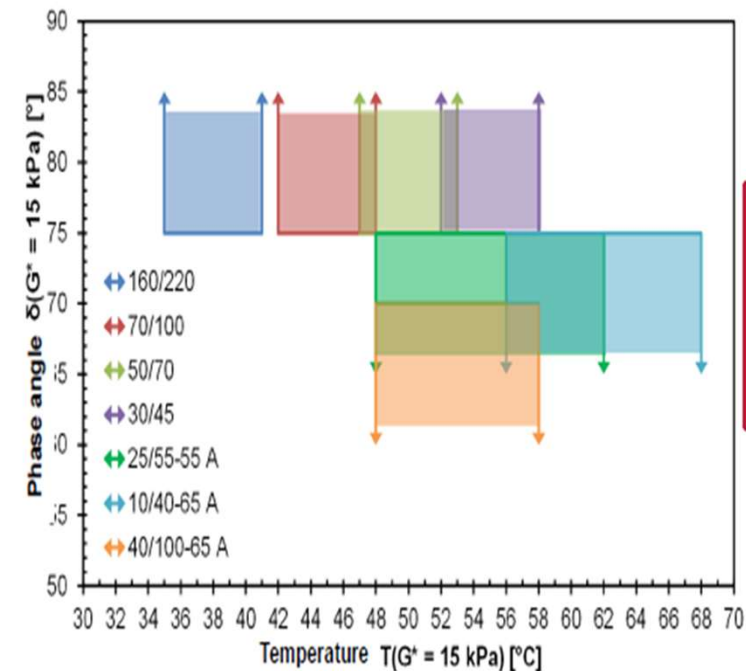


Bitumentypisierung

- Simple identification of binder type and grade
- Effect of polymer modification illustrated
- Experience of softening point R&B can be maintained

European Standards

Graphical visualization of the required values according to ARS 08/2019 in Germany



- $\delta \geq 75 \text{ °}$ → plain asphalt binder
- $\delta \leq 75 \text{ °}$ → polymer modified asphalt binder

T. Spewitz | BTSV – Austausch Dresden | 16. Mai 2024 | 11

Reologia nas especificações como Ensaios Plus com limites

Requirements of the regulations

Entwurf der TL Bitumen-StB, vom 15.09.2023

→ Plain binder

Tabelle 1a: Zusätzliche Anforderungen an die rheologischen Eigenschaften von Straßenbaubitumen

| Merkmal oder Eigenschaft | Einheit | Prüfmethode | Sorten | | | | | |
|-------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------|-----------------------|-----------|-----------|-----------|------------|------------|------------|
| | | | 20/20 | 30/40 | 50/70 | 70/100 | 100/120 | 250/330 |
| Äqui-Schermoduletemperatur $T(G^*=15 \text{ kPa})$ bei 1,59 Hz | °C | TP Bitumen-StB Teil 3 | 55 bis 63 | 52 bis 60 | 48 bis 54 | 43 bis 51 | 35 bis 43 | 30 bis 38 |
| Phasenwinkel $\delta(G^*=15 \text{ kPa})$ bei 1,59 Hz | ° | | ≥ 75 | ≥ 75 | ≥ 75 | ≥ 75 | ≥ 75 | ≥ 75 |
| Beständigkeit gegen Verhärtung unter Einfluss von Wärme und Luft nach DIN EN 12607-1 bei 163 °C | | | | | | | | |
| Zunahme der Äqui-Schermoduletemperatur $T(G^*=15 \text{ kPa})$ | °C | TP Bitumen-StB Teil 3 | ≤ 8 | ≤ 8 | ≤ 9 | ≤ 9 | ≤ 11 | ≤ 11 |
| Abfall des Phasenwinkels $\delta(G^*=15 \text{ kPa})$ | ° | | ≤ 6 | ≤ 6 | ≤ 6 | ≤ 6 | ≤ 6 | ≤ 6 |
| Beständigkeit gegen Verhärtung unter Einfluss von Wärme und Luft nach DIN EN 12607-1 bei 163 °C und beschleunigter Langzeit-Älterung nach DIN EN 14769 bei 100 °C | | | | | | | | |
| Zunahme der Äqui-Schermoduletemperatur $T(G^*=15 \text{ kPa})$ | °C | TP Bitumen-StB Teil 3 | ≤ 18 | ≤ 18 | ≤ 18 | ≤ 18 | ≤ 18 | ≤ 18 |
| Abfall des Phasenwinkels $\delta(G^*=15 \text{ kPa})$ | ° | | ≤ 12 | ≤ 12 | ≤ 12 | ≤ 12 | ≤ 12 | ≤ 12 |
| Verhalten bei tiefen Temperaturen im Biegebalkenrheometer $T(S=300 \text{ MPa})$ $m(S=300 \text{ MPa})$ | °C | TP Bitumen-StB Teil 4 | ≤ -3 | ≤ -6 | ≤ -9 | ≤ -12 | ≤ -15 | ≤ -18 |
| | - | | IA | IA | IA | IA | IA | IA |

IA = Ist anzugeben. Für die Eigenschaft ist vom Hersteller ein Wertebereich zu deklarieren.

T. Spewth | STSV - Ausbauch Dresden | 15. Mai 2024 | 13



ISBS
Institut für Straßenwesen
TU Braunschweig

Fresh binder

Short-term aged binder

long-term aged binder

Temperatura e ângulo de fase equivalentes a 15Pa, medidos no ligante virgem, após RTFOT a após RTFO+ PAV

Requirements of the regulations

Entwurf der TL Bitumen-StB, vom 15.09.2023

→ Polymer modified binder

Tabelle 2a: Zusätzliche Anforderungen an die rheologischen Eigenschaften von Elastomermodifizierten Bitumen (PmB A)

| Merkmal oder Eigenschaft | Einheit | Prüfmethode | Sorten | | | | | |
|-------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------|-----------------------|------------|------------|------------|------------|-------------|--------------|
| | | | 10/40-65 A | 25/55-55 A | 45/80-50 A | 45/80-65 A | 65/105-70 A | 120/200-40 A |
| Äqui-Schermoduletemperatur $T(G^*=15 \text{ kPa})$ bei 1,59 Hz | °C | TP Bitumen-StB Teil 3 | 56 bis 68 | 48 bis 62 | 44 bis 56 | 48 bis 58 | 43 bis 53 | 36 bis 48 |
| Phasenwinkel $\delta(G^*=15 \text{ kPa})$ bei 1,59 Hz | ° | | ≤ 75 | ≤ 75 | ≤ 75 | ≤ 70 | ≤ 70 | ≤ 75 |
| Beständigkeit gegen Verhärtung unter Einfluss von Wärme und Luft nach DIN EN 12607-1 bei 163 °C | | | | | | | | |
| Zunahme der Äqui-Schermoduletemperatur $T(G^*=15 \text{ kPa})$ | °C | TP Bitumen-StB Teil 3 | ≤ 8 | ≤ 8 | ≤ 8 | ≤ 8 | ≤ 8 | ≤ 8 |
| Abfall des Phasenwinkels $\delta(G^*=15 \text{ kPa})$ | ° | | ≤ 6 | ≤ 6 | ≤ 6 | ≤ 6 | ≤ 6 | ≤ 6 |
| Beständigkeit gegen Verhärtung unter Einfluss von Wärme und Luft nach DIN EN 12607-1 bei 163 °C und beschleunigter Langzeit-Älterung nach DIN EN 14769 bei 100 °C | | | | | | | | |
| Zunahme der Äqui-Schermoduletemperatur $T(G^*=15 \text{ kPa})$ | °C | TP Bitumen-StB Teil 3 | ≤ 18 | ≤ 18 | ≤ 18 | ≤ 18 | ≤ 18 | ≤ 18 |
| Abfall des Phasenwinkels $\delta(G^*=15 \text{ kPa})$ | ° | | ≤ 12 | ≤ 12 | ≤ 12 | ≤ 12 | ≤ 12 | ≤ 12 |
| Verhalten bei tiefen Temperaturen im Biegebalkenrheometer $T(S=300 \text{ MPa})$ $m(S=300 \text{ MPa})$ | °C | TP Bitumen-StB Teil 4 | ≤ -9 | ≤ -12 | ≤ -15 | ≤ -15 | ≤ -18 | ≤ -18 |
| | - | | IA | IA | IA | IA | IA | IA |

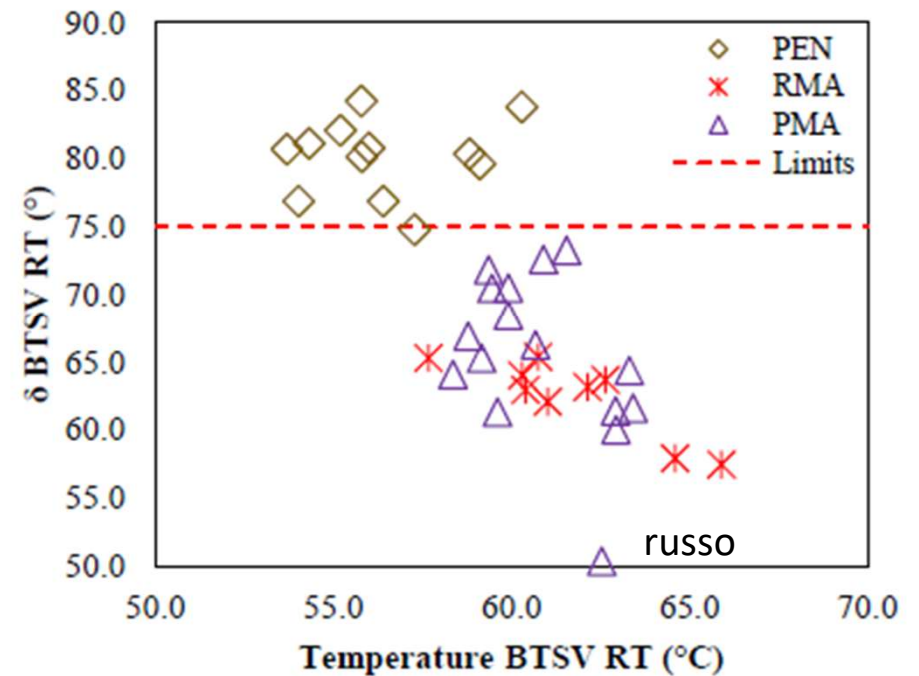
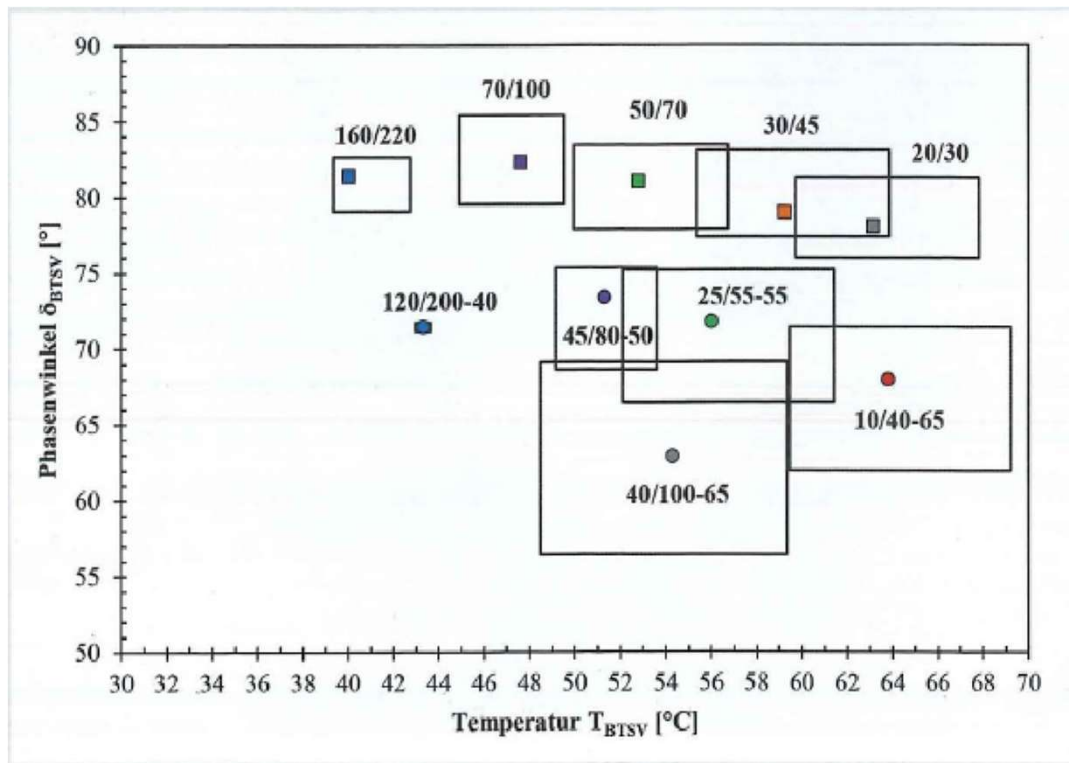
IA = Ist anzugeben. Für die Eigenschaft ist vom Hersteller ein Wertebereich zu deklarieren.

T. Spewth | STSV - Ausbauch Dresden | 15. Mai 2024 | 14

BTSV

Os 37 ligantes do projeto DNIT

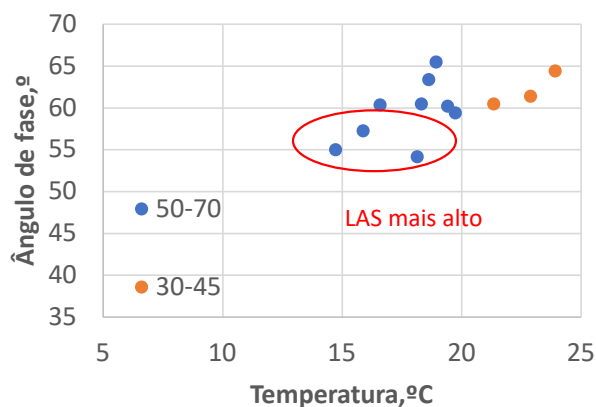
➤ Parâmetro de alta temperatura intermediária – especificado na Alemanha



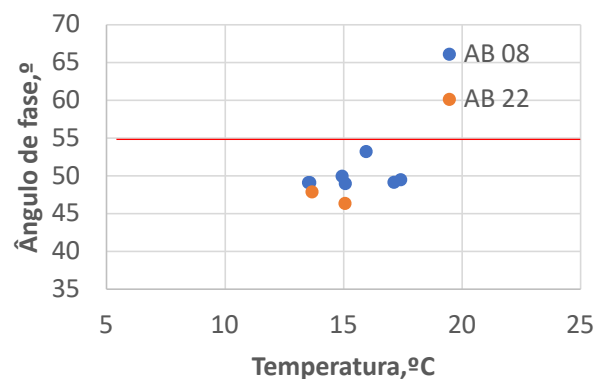
➤ Parâmetro de temperatura intermediária em estudo

Linha de boa resistência a fadiga em ângulo de fase de 55°

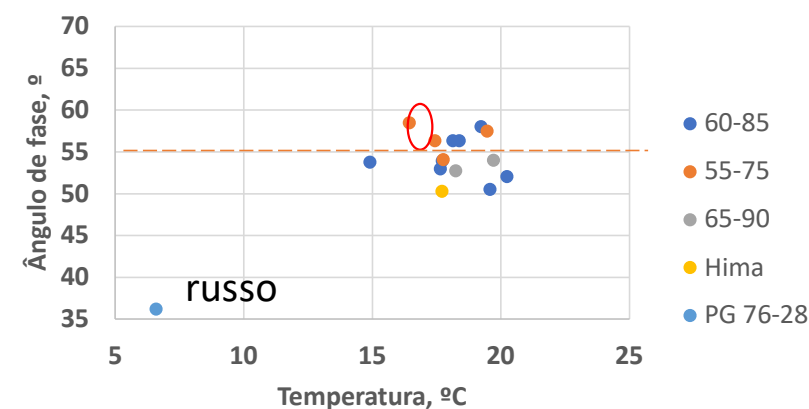
BTSV CAP - temp intermediária



BTSV AB Temperatura intermediária



BTSV AMP Temperatura intermediária



Acima de 55° são os piores valores de LASFFL, menor que 1,5 para AMP 55-75 e alguns 60-85

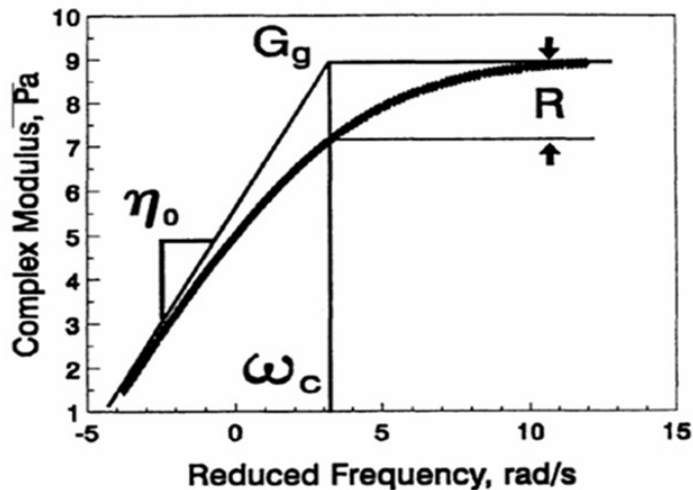
Índices reológicos dos EUA - FADIGA

NCHRP 09-59 (2022) - R e GRP com limites

$$R = \log(2) \frac{\log\left(\frac{S}{8.000}\right)}{\log(1-m)}$$

Resultados do BBR

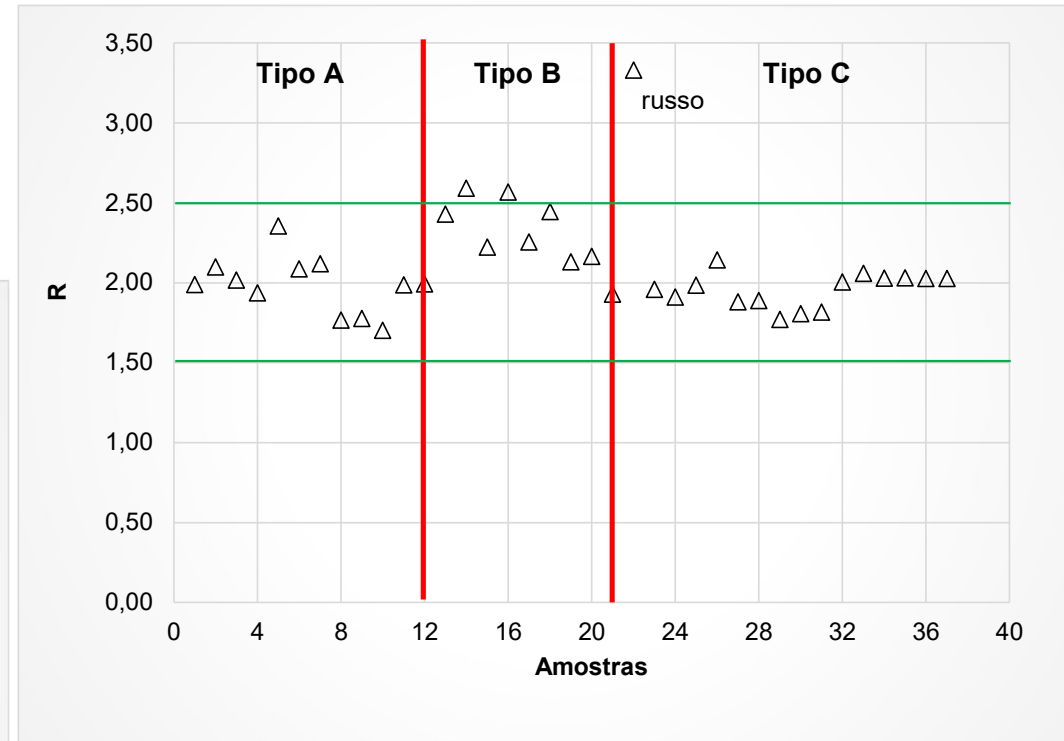
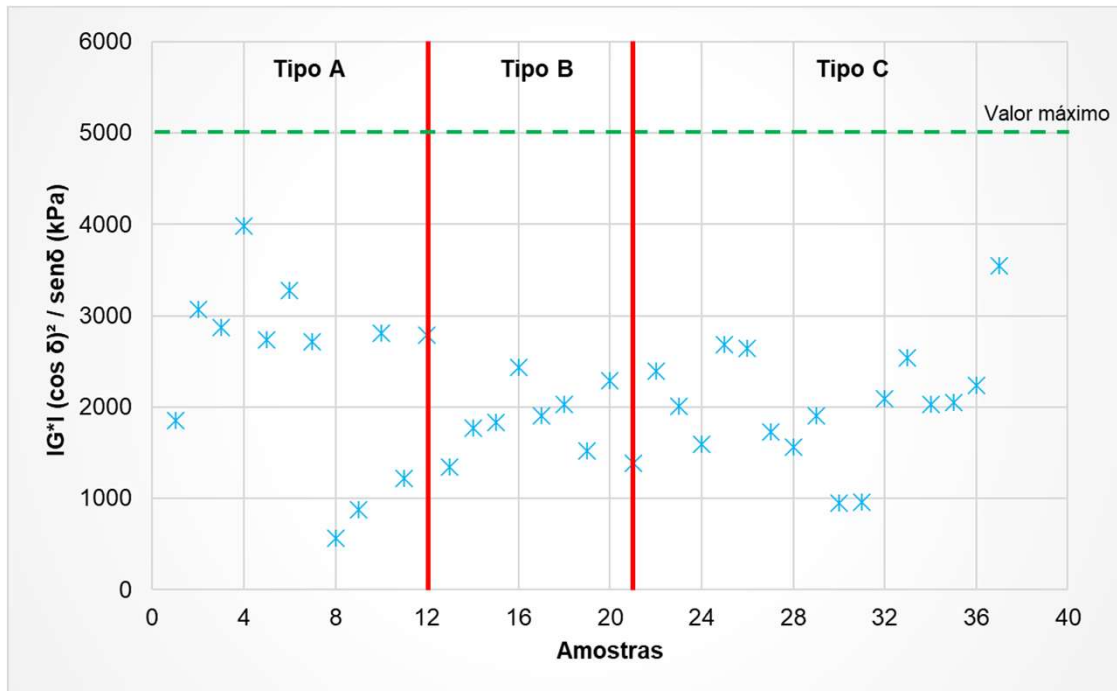
Limites de 1,5 a 2,5 (20h PAV)



| PG de baixa temperatura | temperaturas de ensaio propostas (°C) |
|-------------------------|---------------------------------------|
| -46 | 15 |
| -30 | 17 |
| -34 | 19 |
| -28 | 22 |
| -22 | 25 |
| -16 | 27 |
| -10 | 29 |

O requisito $|G^*| \sin \delta$ deve ser substituído pelo parâmetro Glover-Rowe ($GRP = |G^*| \cos^2 \delta / \sin \delta$), devendo ser determinado na frequência de 10 rad/s. O valor máximo para GRP após envelhecimento no RTFOT seguido do PAV 20 horas deve ser 5.000 kPa.

GRP e R (NCHRP 9-59) - 2022



Delta Tc – índice de trincamento

$$T_{c,s} = T_1 + \left(\frac{(T_1 - T_2) * (\text{Log } 300 - \text{Log } S_1)}{\text{Log } S_1 - \text{Log } S_2} \right) - 10$$

$$T_{c,m} = T_1 + \left(\frac{(T_1 - T_2) * (0.300 - m_1)}{m_1 - m_2} \right) - 10$$

where,

S_1 = creep stiffness at T_1 , MPa,

S_2 = creep stiffness at T_2 , MPa,

m_1 = creep rate at T_1 ,

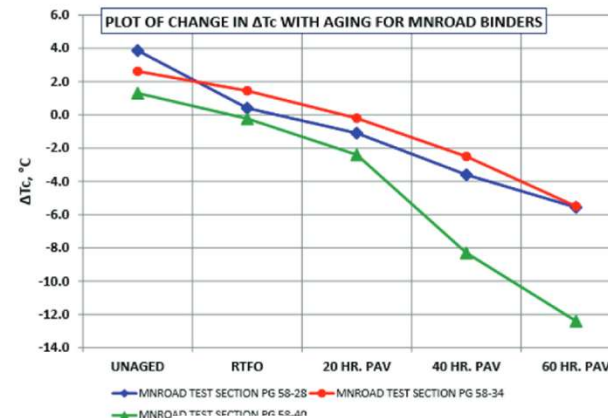
m_2 = creep rate at T_2 ,

T_1 = temperature at which S and m passes, °C

T_2 = temperature at which S and m fails, °C.

Therefore, the equation for ΔT_c becomes:

$$\Delta T_c = T_{c,s} - T_{c,m}$$



Delta Tc ≥ -5 ou -2,5
dependente do tempo de PAV

➤ Unmodified, Polymer-modified, ReOB-modified, SDA, PPA-modified, Biophalt, Oxidized, Airblown, Visbroken.

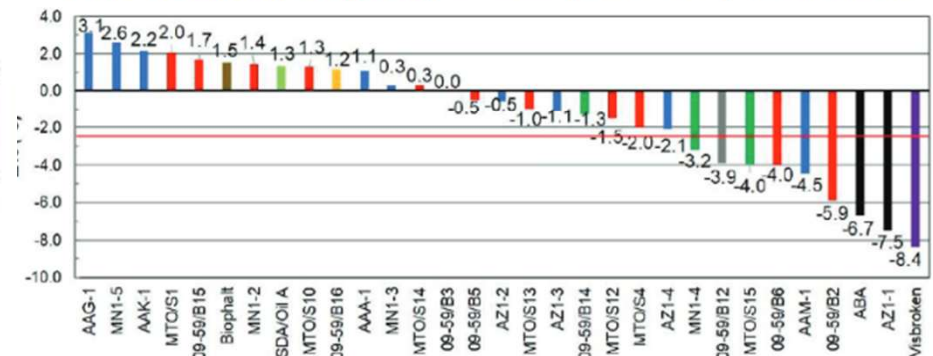
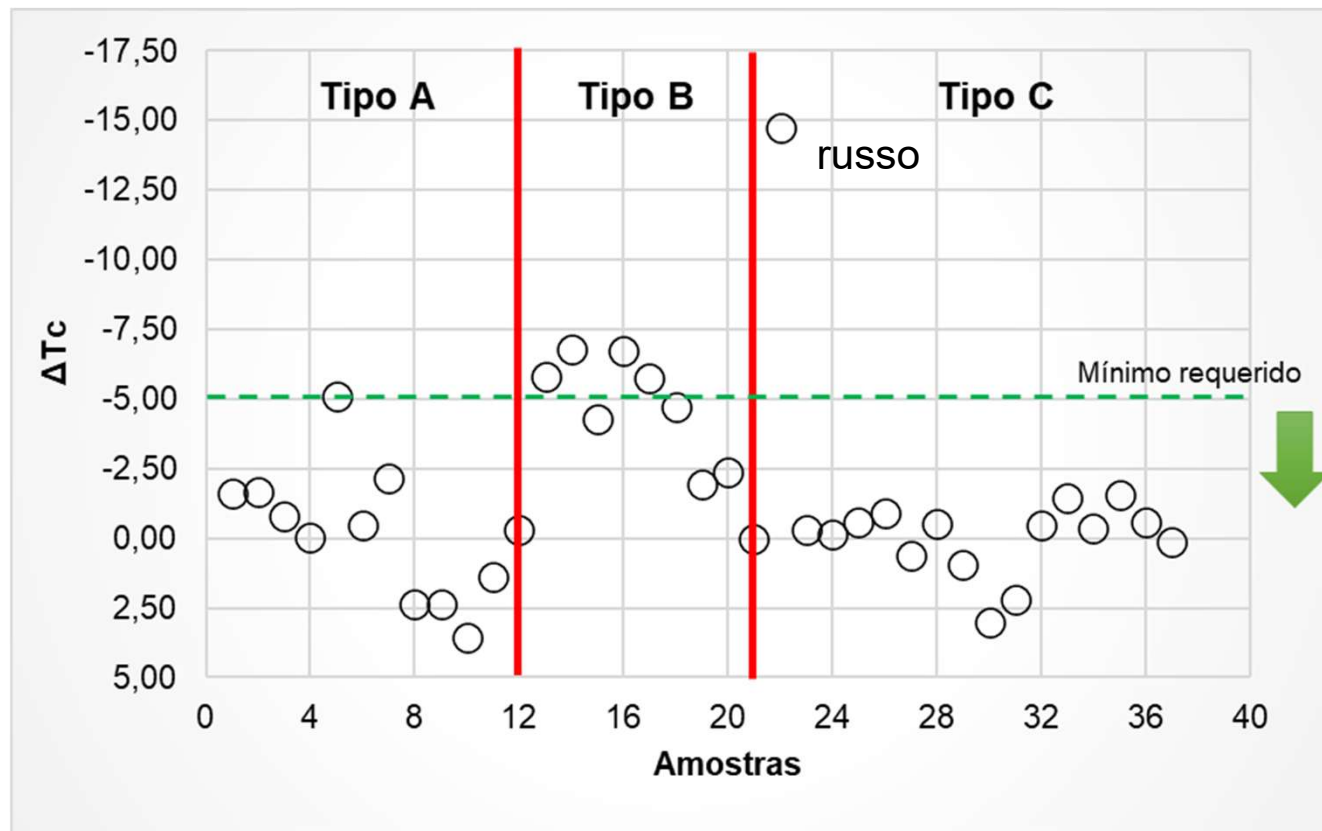
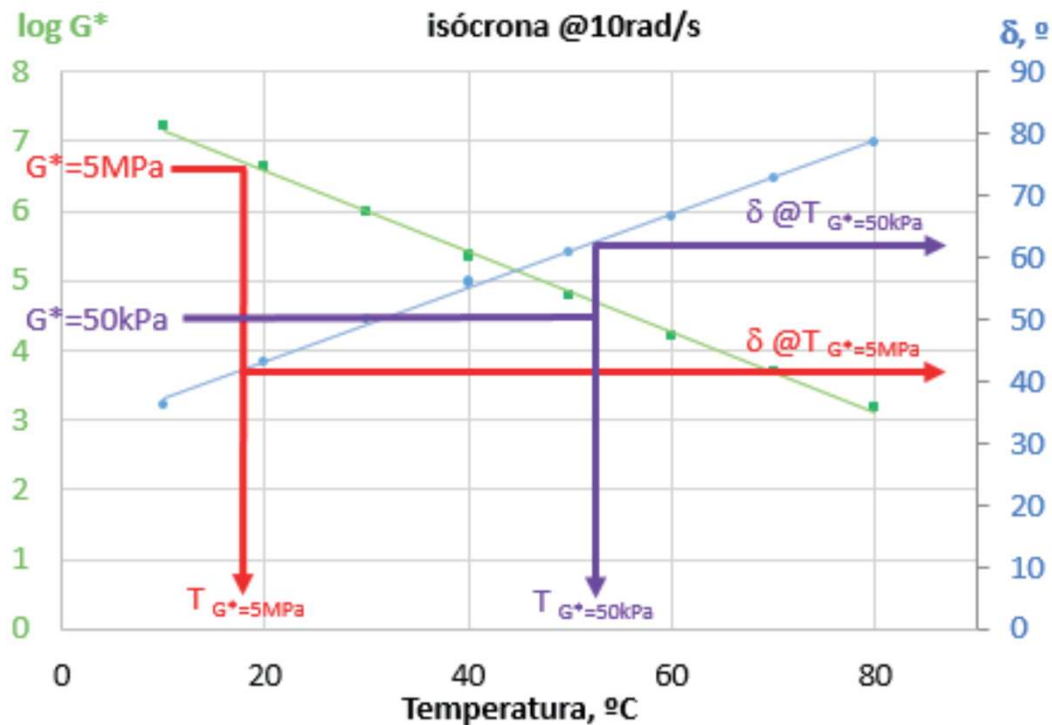


Figure 11. ΔT_c (PAV20) of Various Binders from NCHRP 9-60 Research Project Database (4)

Delta Tc

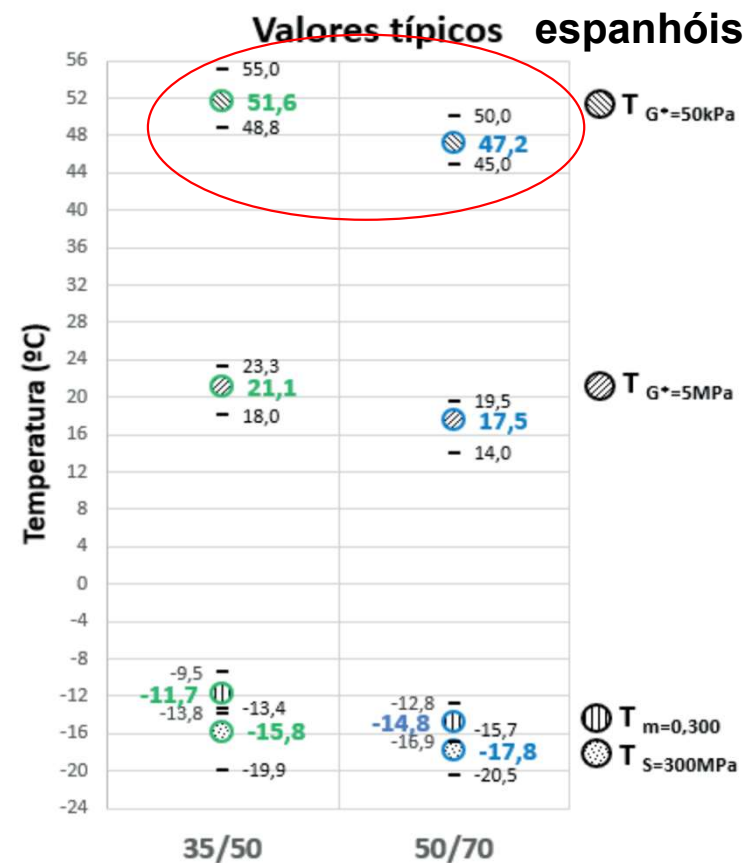
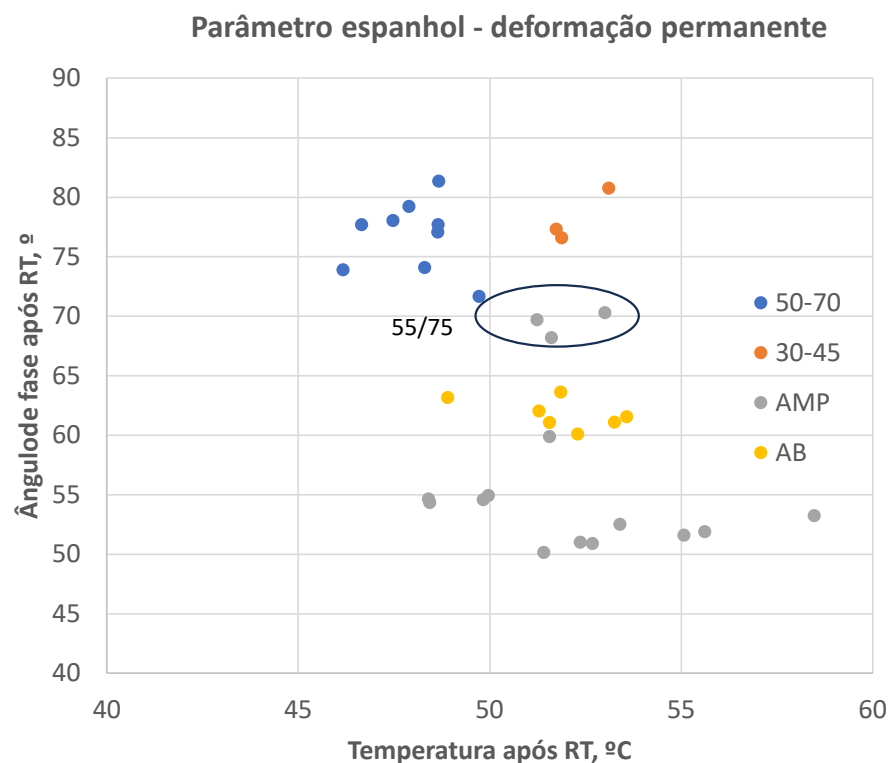


Parâmetros espanhóis – fadiga e deformação permanente



El ensayo DSR descrito en la norma EN 14770, se basa en aplicar un esfuerzo cortante constante oscilatorio a una muestra de ligante colocada entre dos platos metálicos paralelos. El ensayo se realiza a temperaturas de 10°C a 80°C) a frecuencias entre 0,1 Hz y 10 Hz. **Las temperaturas a las cuales $G^*= 5 \text{ MPa}$ y $G^*= 50 \text{ kPa}$ se obtienen mediante interpolación logarítmica en la isócrona a una frecuencia de 1,59 Hz, de G^* vs T. Los ángulos de fase correspondientes se obtienen por interpolación lineal de las temperaturas obtenidas en la curva de δ vs. T a dicha frecuencia.**

Parâmetros espanhóis CAP deformação permanente



G* a 15°C a 10Hz

| Propiedad | Unidad | Método de ensayo | Dato |
|--------------------------------------------------|--------|------------------|------|
| TS= 300 MPa, medida por el BBR(a) | °C | EN 14771 | TBR |
| Tm=0,3, medida por el BBR(a) | °C | EN 14771 | TBR |
| G* a 15 °C y 10 Hz medido mediante DSR(b) | MPa | EN 14770 | TBR |
| TG*/senδ = 1 kPa a 1,6 Hz medido mediante DSR(b) | °C | EN 14770 | TBR |

a BBR = Reómetro de Flexión.

b DSR = Reómetro de corte dinámico (Dynamic Shear Rheometer) o cualquier otro reómetro capaz de medir un módulo complejo.

TABLE 9/8: (05/18) Binder Characteristics to be Reported

| Characteristic | Test Method | Unit | Binder for EME2 | FPC frequency | | |
|-------------------------------------------------|-------------|-------------------|-----------------|---------------|-----|-----|
| | | | | AS | STA | LTA |
| Brookfield Viscosity T 200cP | EN 13302 | °C | TBR | A | | |
| T 2000cP | | °C | TBR | | A | |
| T 5000cP | | °C | TBR | | A | |
| G* and Phase Angle | BS EN 14770 | Pa, degrees | TBR | A | A | A |
| VET temperature, G'=G'', at 0.4 Hz | | °C | TBR | A | A | A |
| G* at the VET temperature | | Pa | TBR | A | A | A |
| G' and G'' Mastercurves 80°C to 0°C | | Graphical Output | TBR | A | A | A |
| G'' and Phase Angle at 15°C, 10Hz and 20°C, 1Hz | | Pa, degrees | TBR | A | A | A |
| T _{g=300 MPa} , by BBR | BS EN 14771 | °C | TBR | A | A | A |
| T _{m=0.3} , by BBR | | °C | TBR | A | A | A |
| Pendulum Cohesion, min | BS EN 13588 | J/cm ² | TBR | A | A | A |
| Fraass breaking point, min | EN 12593 | °C | TBR | | A | |

Notes:

AS = As Supplied; STA = After EN 12607-1 (RTFOT) * LTA = After PAV85 *

* An ageing profile determined in accordance with clause 955 is an acceptable alternative to STA and PAV85.

All tests to be carried out on sub-samples of a single bulk sample of binder.

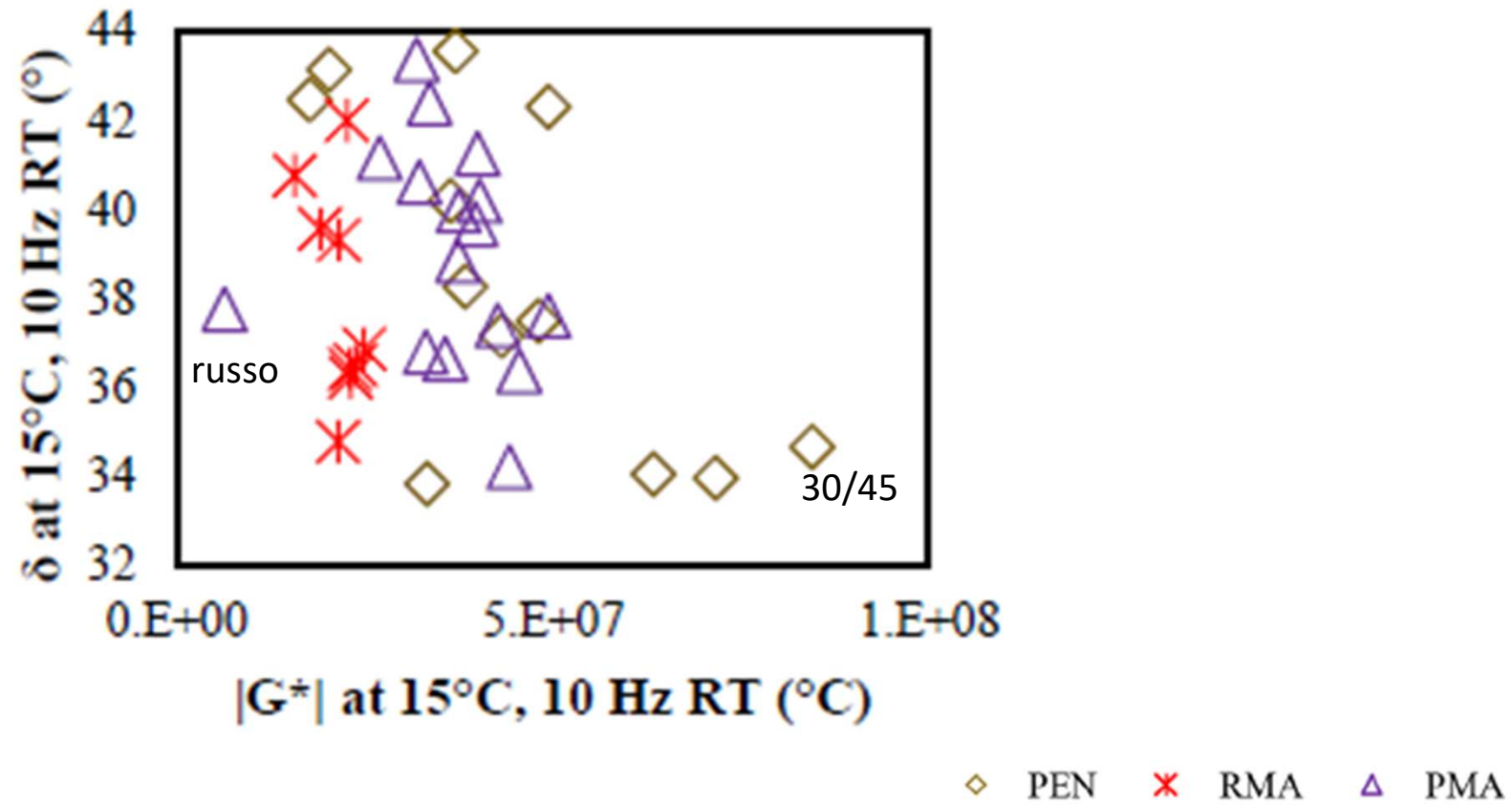
Minimum test frequency : A = Annually.

(Indicated frequencies apply only if product is in regular supply.)

Proposta espanhola e inglesa BS

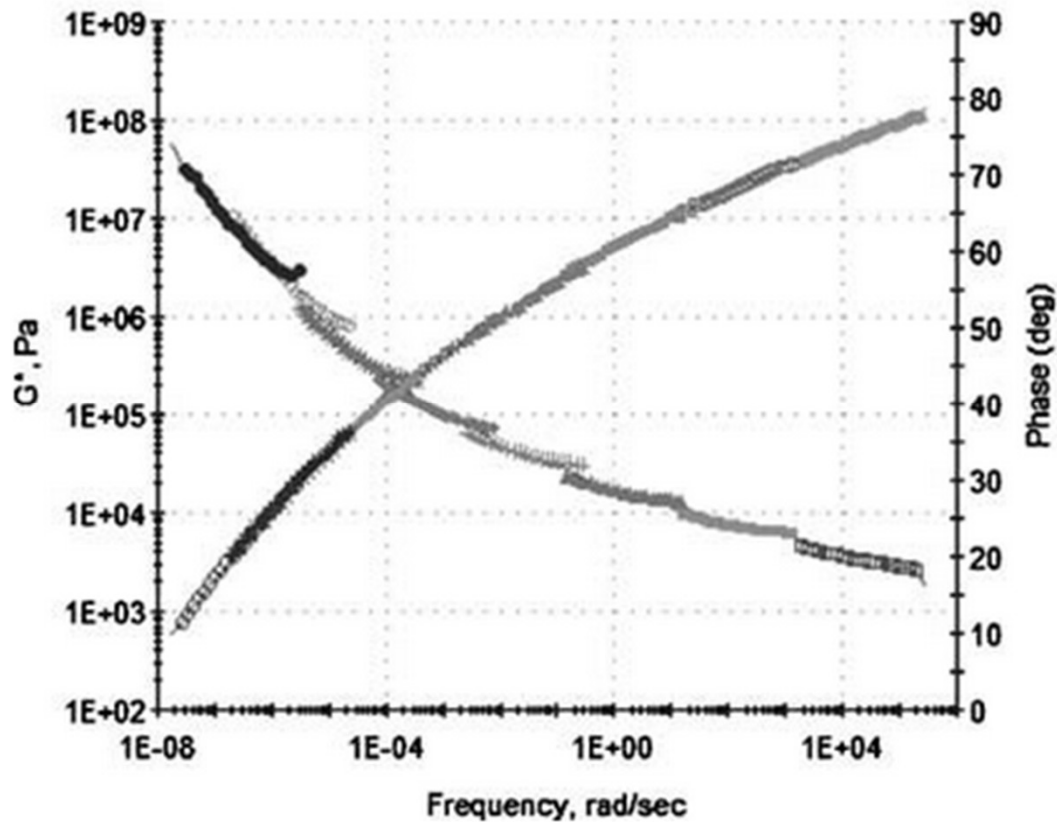
| Binder for EME2 | | | | FPC frequency | | |
|-------------------------------------------------|------------------------------------------------------|------------------|-----|---------------|------|------|
| Characteristic | Test method | Unit | | AS | STA | LTA |
| Brookfield viscosity T200cP | BS EN 13302 | °C | TBR | A | | |
| T2000cP | | °C | TBR | | A | |
| T5000cP | | °C | TBR | | A | |
| G* and phase angle | BS EN 14770 see Clause 956 Graphical output | Pa, degrees | TBR | A | A | A |
| VET temperature, G'=G'', at 0.4 Hz | | °C | TBR | A | A | A |
| G* at the VET temperature | | Pa | TBR | A | A | A |
| G' and G'' mastercurves 80°C to 0°C | | Graphical output | TBR | A | A | A |
| G'' and phase angle at 15°C, 10Hz and 20°C, 1Hz | | Pa, degree | TBR | A | A | A |
| Ts=300MPa by BBR | BS EN 14771 | °C | TBR | A(Q) | A(Q) | A(Q) |
| Tm=0.3, by BBR | | °C | TBR | A(Q) | A(Q) | A(Q) |

G^* a 15°C

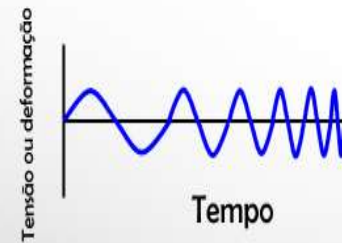


Curva mestre

Varredura de frequência



VARREDURA DE FREQUENCIA

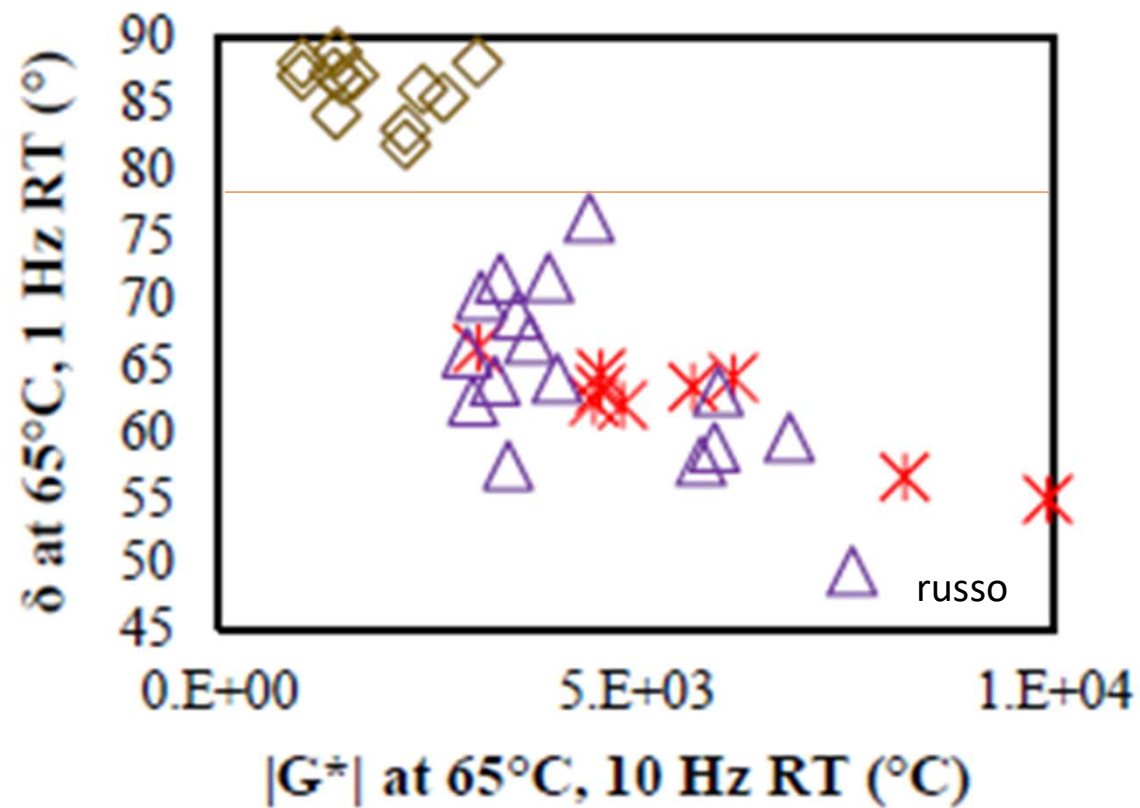


Resposta do material ao aumento de frequência é monitorado à amplitude constante (tensão ou deformação) e temperatura.

USOS

- Propriedades – módulos a carregamentos curtos e longos
- Extensão do tempo ou faixa de frequência com TTS – superposição de tempo e temperatura

AF a 65°C, 1Hz após RT x G^* a 65°C, 10 Hz após RT



Conclusões - Ensaio reológicos

Índices que distinguem ligantes modificados dos não modificados

- BTVS;
- AF a 65°C, 1 Hz após RT X G* a 65°C a 10 Hz após RT;
- Parâmetro espanhol AF e Temperatura após RT (50 KPa);
- Asfalto russo é sempre visto como outlier;
- G* a 15°C a 10 Hz;
- R, GRP e delta Tc não parecem ser interessantes de ser explorados

Outros ensaios para misturas quentes

Especificação australiana – parâmetro de resistência a deformação permanente

Asfalto modificado 2020

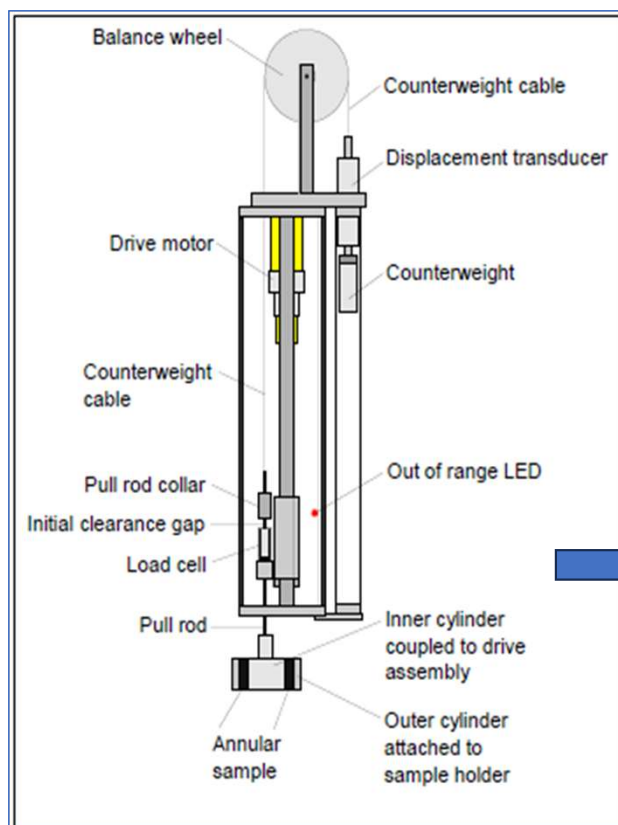


Table 8.2: Properties of Polymer Modified Binders for Asphalt Applications

| Test method | Class Binder property | A35P | A25E | A20E | A15E | A10E |
|-------------------------------------------|----------------------------------------------------|--------------------|-------|-------|--------|--------|
| AS/NZS 2341.4 or AGPT/T111 ⁽¹⁾ | Viscosity at 165 °C (Pa.s) max. ⁽¹⁾ | 0.6 | 0.6 | 0.6 | 0.9 | 1.1 |
| AGPT/T122 | Torsional recovery at 25 °C, 30 s (%) | 6–21 | 17–30 | 38–70 | 55–80 | 60–86 |
| AGPT/T131 | Softening point (°C) | 62–74 | 52–62 | 65–95 | 82–105 | 88–110 |
| AGPT/T125 | Stress ratio at 10 °C min. | TBR ⁽²⁾ | TBR | TBR | TBR | TBR |
| AGPT/T121 | Consistency 6% at 60 °C (Pa.s) min. ⁽³⁾ | 1000 | 400 | 500 | 900 | 1000 |
| AGPT/T121 | Stiffness at 25 °C (kPa) max. | 120 | 45 | 35 | 30 | 30 |
| AGPT/T108 | Segregation (%) max. | 8 | 8 | 8 | 8 | 8 |
| AGPT/T112 | Flash point (°C) min. | 250 | 250 | 250 | 250 | 250 |
| AGPT/T103 | Loss on heating (% mass) max. | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |

Especificação australiana – parâmetro de resistência a fadiga - taxa de tensão a 10°C
 Asfalto modificado 2020

Razão de tensão= Tensão (10 def.)/Tensão (3 def.)

Figure 9.1: Distressed binder after testing

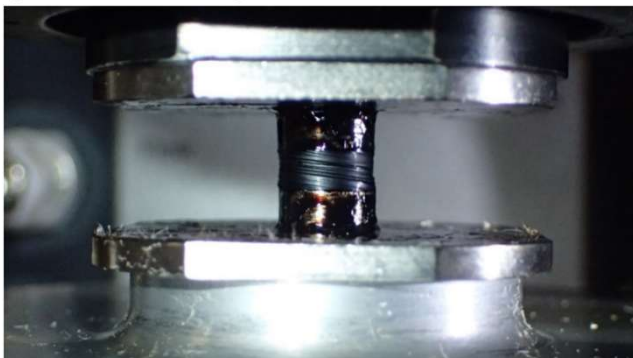
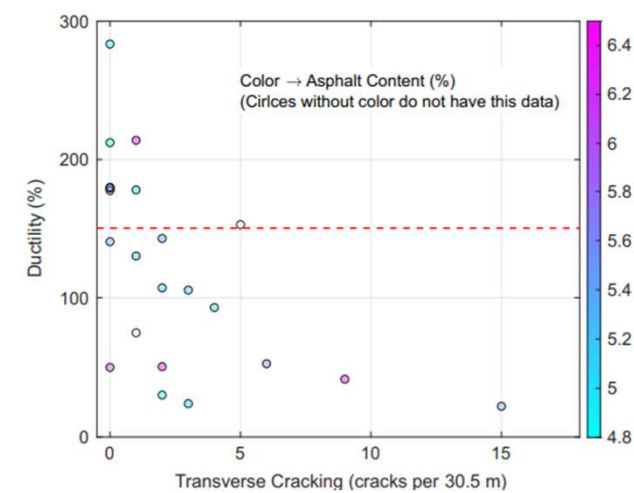
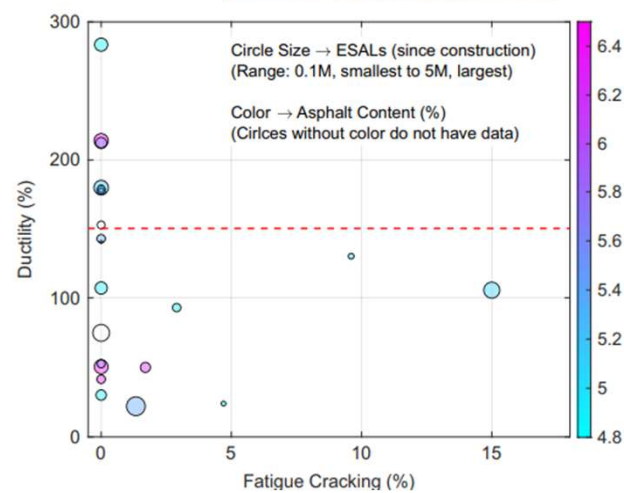
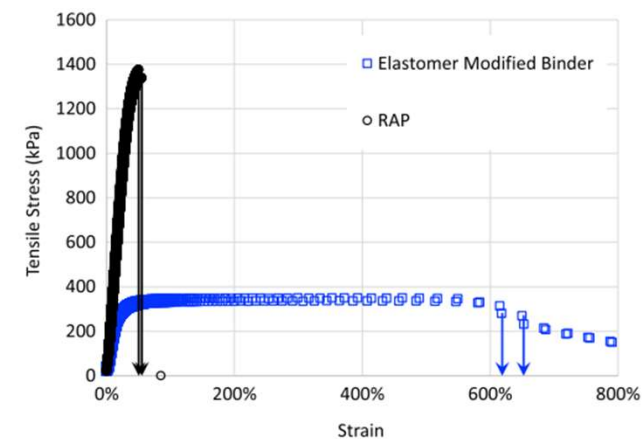


Table 8.2: Properties of Polymer Modified Binders for Asphalt Applications

| Test method | Class Binder property | A35P | A25E | A20E | A15E | A10E |
|-------------------------------------------|----------------------------------------------------|--------------------|-------|-------|--------|--------|
| AS/NZS 2341.4 or AGPT/T111 ⁽¹⁾ | Viscosity at 165 °C (Pa.s) max. ⁽¹⁾ | 0.6 | 0.6 | 0.6 | 0.9 | 1.1 |
| AGPT/T122 | Torsional recovery at 25 °C, 30 s (%) | 6–21 | 17–30 | 38–70 | 55–80 | 60–86 |
| AGPT/T131 | Softening point (°C) | 62–74 | 52–62 | 65–95 | 82–105 | 88–110 |
| AGPT/T125 | Stress ratio at 10 °C min. | TBR ⁽²⁾ | TBR | TBR | TBR | TBR |
| AGPT/T121 | Consistency 6% at 60 °C (Pa.s) min. ⁽³⁾ | 1000 | 400 | 500 | 900 | 1000 |
| AGPT/T121 | Stiffness at 25 °C (kPa) max. | 120 | 45 | 35 | 30 | 30 |
| AGPT/T108 | Segregation (%) max. | 8 | 8 | 8 | 8 | 8 |
| AGPT/T112 | Flash point (°C) min. | 250 | 250 | 250 | 250 | 250 |
| AGPT/T103 | Loss on heating (% mass) max. | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |

Dutibilidade Pocker chip – parâmetro de resistência a fadiga - TEXAS



DOT Texas - e DSR ao invés de BBR com placa 8mm

LOW TEMPERATURE DYNAMIC SHEAR RHEOMETER TESTING OF ASPHALT BINDER

TxDOT DESIGNATION: TEX-554-C

Test Procedure for

LOW TEMPERATURE DYNAMIC SHEAR RHEOMETER TESTING OF ASPHALT BINDER



TxDOT Designation: Tex-554-C

Effective Date: October 2024



- Condicionar amostra a PG +10°C) for 2100 s;
- Testar amostra em placa 8mm com taxa de deformação de 1% na frequência angular de 10 c/s;
- Reportar a média G^* e δ nos últimos 5 ciclos.

DENT – AASHTO 425-23 – parâmetro de fadiga

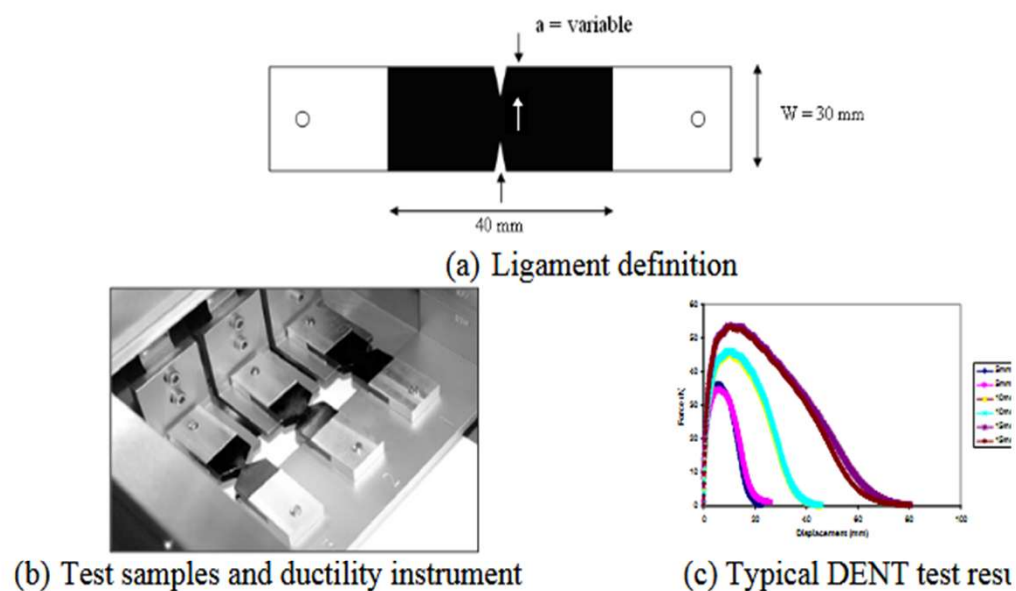


Figure 10. FHWA DENT Test (28).

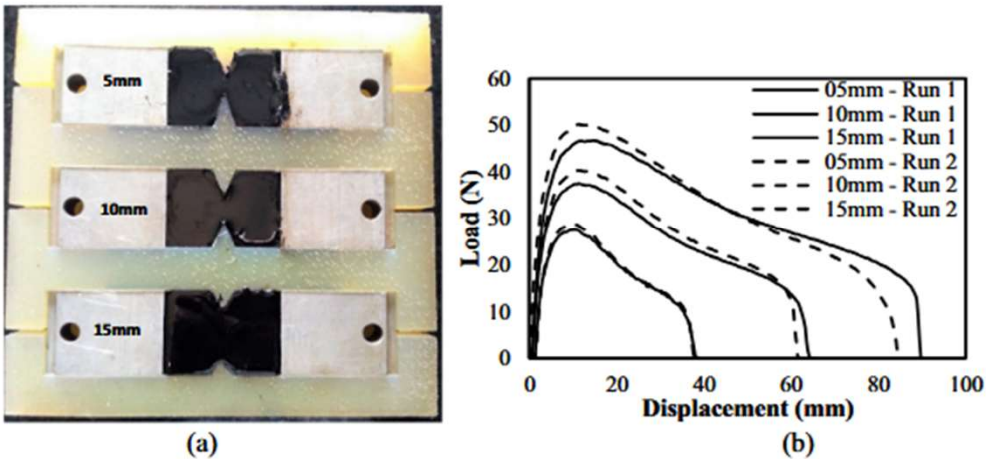


Fig. 2. (a) Silicon mold having 5 mm, 10 mm & 15 mm notch length (b) typical load displacement curve.

Parâmetros de desempenho para mistura a frio

Emulsões – PG (NCHRP) Inicialmente NCU

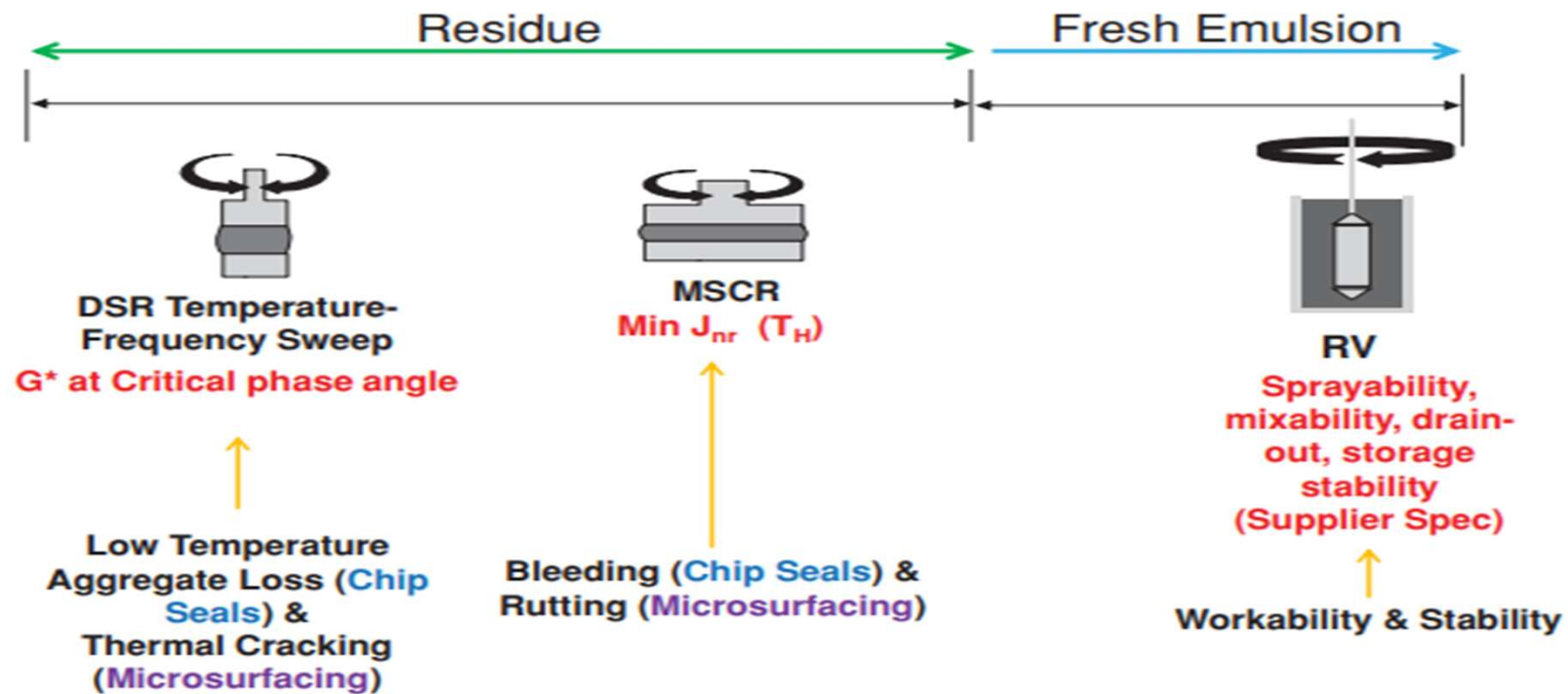


Figure 2.1. Recommended EPG specification tests for emulsions.

NCHRP 09-63: A Calibrated and Validated National Performance Related Specification for Emulsified Asphalt Binder

Projetos de campo: 2019-2020

Field Projects 2020-22

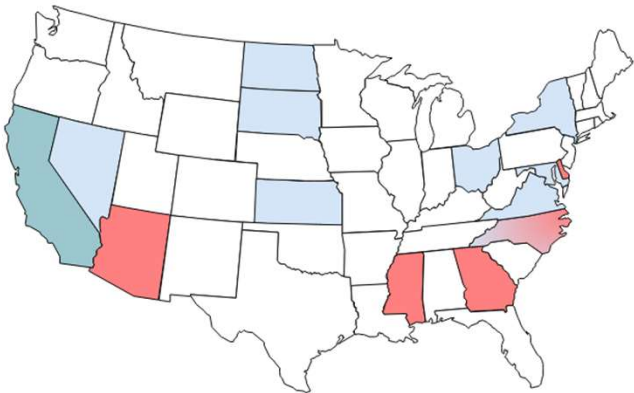
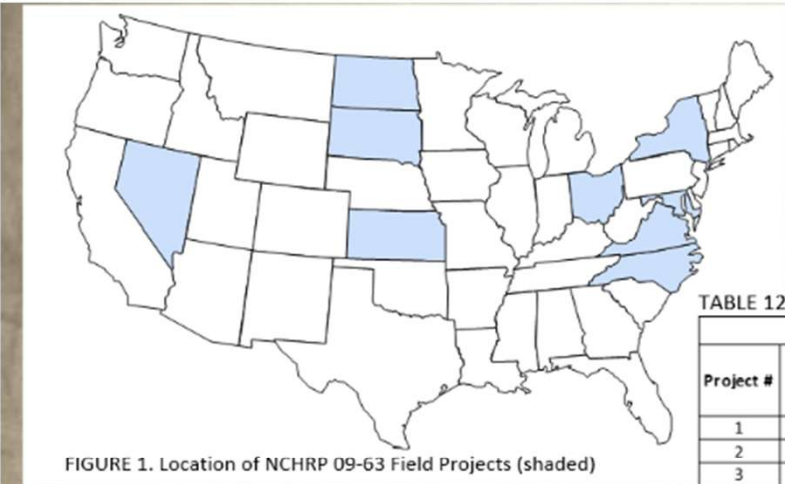


TABLE 12. Field Experiment Projects

| PROJECT INFO | | | | | | |
|--------------|----------------|--------------|-------|------------------|--------------------------|--------------------------|
| Project # | Route/Street | City/Town | State | Agency | Type | Actual Construction Date |
| 1 | Rt. 80 | Sherburne | NY | NYS DOT | Chip Seal w/Fog and Sand | 9/6/2019 |
| 2 | RT. 11 | Homer | NY | NYS DOT | Chip Seal w/Fog and Sand | 7/17/2020 |
| 3 | Padgett Rd. | Union Mills | NC | Rutherford Co. | Double Chip Seal | 7/22/2020 |
| 4 | Rt. 9B | Rouses Point | NY | NYS DOT | Double Microsurfacing | 8/10/2020 |
| 5 | SR 117 | Belle Center | OH | OHDOT | Microsurfacing | 8/20/2020 |
| 6 | CR 2 | Colgan | ND | Divide Co. | Microsurfacing | 8/27/2020 |
| 7 | US 85 | Fortuna | ND | NDDOT | Chip Seal w/Fog | 8/28/2020 |
| 8 | Norris Peak Rd | Rapid City | SD | Pennington Co. | Chip Seal w/Fog | 9/1/2020 |
| 9 | US 6 | Dyer | NV | NVDOT | Chip Seal w/Fog and Sand | 9/10/2020 |
| 10 | SW Gage Blvd | Topeka | KS | Mission Township | Chip Seal | 9/17/2020 |
| 11 | CR 660 | Farmville | VA | Cumberland Co. | Double Chip Seal | 9/21/2020 |
| 12 | Beulah Road | Vienna | VA | VDOT | Microsurfacing | 9/22/2020 |
| 13 | Arrants Road | North East | MD | Cecil Co. | Slurry Seal | 9/25/2020 |

Task Force

Classificação da emulsão - EPG

■ Examples of chip seals EPG

Classification of
emulsified asphalt
performance

Workability index of
emulsified asphalt

Residue high and
low temperature
index

| Existing Emulsion Name | Proposed EPG Grade | | Fresh Emulsion Tests | | | | Residual Binder Tests | | Pass & Grade or Fail at Test Temp/ Traffic Level | |
|------------------------|--------------------|-------|----------------------|----------|----------|----------|-----------------------|-------------------|--------------------------------------------------|---------------|
| | | | | | | | | | | |
| CRS-2 (NC) | CRS-EPG67-19L | | | | | | | | | |
| CRS-2L (F) | CRS | 67-19 | Low | 1.1 Pass | 1.0 Pass | 180 Pass | 350 Pass | 6.75 Pass at Low | 14 Pass at Low | CRS-EPG67-19L |
| | | | Med | | | | | 6.75 Fail at Med | 14 Pass at Med | Fail |
| | | | High | | | | | 6.75 Fail at High | 14 Fail at High | Fail |
| CRS-2P (A) | CRS | 67-19 | Low | 0.3 Pass | 1.0 Pass | 80 Pass | 450 Pass | 2.5 Pass at Low | 4 Pass at Low | CRS-EPG67-19L |
| | | | Med | | | | | 2.5 Pass at Med | 4 Pass at Med | CRS-EPG67-19M |
| | | | High | | | | | 2.5 Pass at High | 4 Pass at H | from NCHRP833 |

from NCHRP837

Emulsão catiônica ruptura rápida
Temperatura pavimento 67-19
Baixo tráfego

EUA e Africa do Sul - requisitos de desempenho preliminares

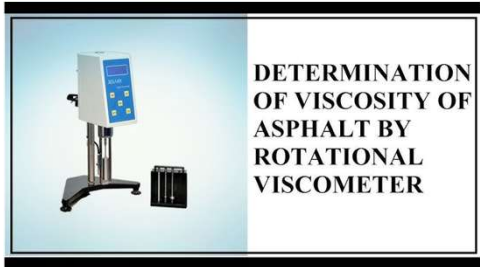
África do Sul

| Engineering Property | Test Method | Parameter(s) Measured |
|--------------------------------------------------------------|--------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| Tests on Fresh Emulsion Properties (Constructability) | | |
| Storage Stability | Modified ASTM D6930 – Settlement and Sedimentation | <ul style="list-style-type: none"> Rotational Viscosity, η, B-24-hour Separation Ratio (R_s) C-24-hour Stability Ratio (R_d) |
| Sprayability | Modified AASHTO TP48 - Rotational Viscometer | <ul style="list-style-type: none"> Rotational Viscosity, η, @ high shear at (XX 1/sec) |
| Drain-Out | Modified AASHTO TP48-Rotational Viscometer | <ul style="list-style-type: none"> Rotational Viscosity, η, @ low shear rate (XX 1/sec) |
| Resistance to Early Raveling /Curing | AASHTO TP 91-11 Bitumen Bond Strength (BBS) | <ul style="list-style-type: none"> A-Minimum Pull-Out Tensile Strength (POS) @ XX hrs. of Curing Time |
| Residue Recovery Method: ASTM D7497 Method B | | |
| Resistance to Bleeding and Flushing | Multiple Stress Creep and Recovery Test (AASHTO TP 70) | <ul style="list-style-type: none"> J_w Stress Sensitivity |
| Resistance Raveling | Bitumen Bond Strength Test (AASHTO TP-91) | <ul style="list-style-type: none"> Wet and Dry Pull-off Bond Strength Moisture Damage ratio |
| | DSR-Linear Amplitude Test | <ul style="list-style-type: none"> Strain at maximum Stress |
| Early Fatigue | Linear Amplitude Sweep Test (LAS) | <ul style="list-style-type: none"> Number of Cycles to failure (N_f) at specified % Strain |
| Polymer Identifier | Elastic Recovery DSR | <ul style="list-style-type: none"> % recovery |
| Tests on PAV Aged (AASHTO R28) Materials | | |
| Late Fatigue | Linear Amplitude Sweep Test (LAS) | <ul style="list-style-type: none"> Cycles to failure (N_f) at specified % Strain Aging Susceptibility |
| Resistance to Thermal Cracking | DSR Frequency Sweep to estimate BBR properties. | <ul style="list-style-type: none"> Estimated $S(60)$, $m(60)$ |

EUA

| Property | Test Method | Parameter(s) Measured |
|--------------------------------|----------------------------------------------------|---------------------------------------------------------------------------------------------------------------|
| Storage Stability ^a | Modified ASTM D6930 – Settlement and Sedimentation | A Rotational viscosity, η B 24-hour separation ratio (R_s) C 24-hour stability ratio (R_d) |
| Sprayability ^b | Modified AASHTO TP 48 – Rotational Viscometer | Rotational viscosity, η , @ high shear rate |
| Drainout ^b | Modified AASHTO TP 48 – Rotational Viscometer | Rotational viscosity, η , @ low shear rate |
| Mixability ^c | Modified AASHTO TP 48 – Rotational Viscometer | Rotational viscosity, η , @ 5 rpm |
| Curing Time ^d | Modified ASTM D3121 – Rolling Ball Test | Rolling distance, time to 25 cm rolling distance |

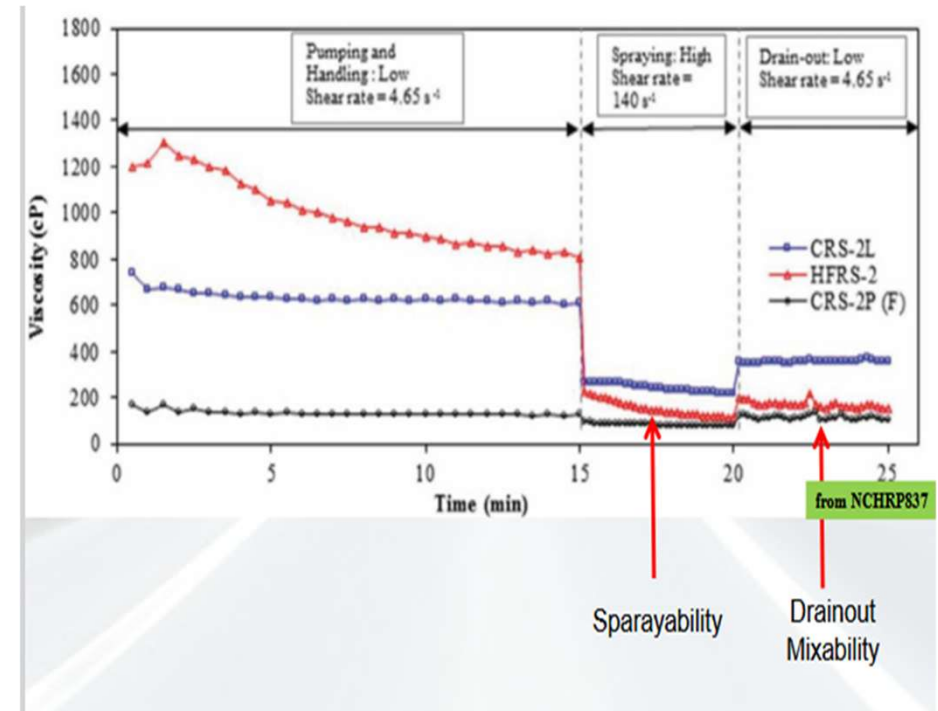
| Performance Characteristic | Test Method | Parameter(s) Measured |
|-----------------------------------------|----------------------------------------------|------------------------------------------------------------------------------------------------------------------------------|
| Rutting at High-temperature EPG | Multiple Stress Creep and Recovery Test | <ul style="list-style-type: none"> Non-recoverable Creep Compliance, J_{tr} |
| Thermal Cracking at Low-temperature EPG | Dynamic Shear Rheometer Frequency Sweep Test | <ul style="list-style-type: none"> Dynamic Shear Modulus (G^*) at $\delta_{critical}$ |



Trabalhabilidade

Simulação do processo de aplicação

| Testes na emulsão virgem - propriedades de trabalhabilidade | | |
|-------------------------------------------------------------|-------------------------|--------------------------------|
| Propriedade | Método | Parâmetro medido |
| Pulverizabilidade | AASHTO TP 48 modificado | viscosidade rotacional 150 rpm |
| Drenagem TS | | viscosidade rotacional 5 rpm |
| Mixabilidade Micro | | viscosidade rotacional 5rpm |



Etapa 1 – Emulsão no tanque – manuseio e bombeamento - 5 rpm

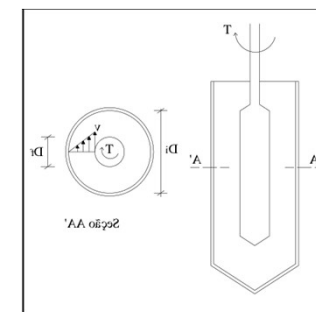
Etapa 2 – Pulverização da emulsão (TS) – 150 rpm

Etapa 3 – Drenagem (TS) e Mixabilidade (Micro) na superfície do pavimento- 5rpm

Trabalhabilidade

Testes na emulsão virgem - propriedades de trabalhabilidade

| Propriedades | Método | Parâmetro medido |
|----------------------------|------------------------------------------------------------|-----------------------------------------------------------------------------------------|
| Estabilidade à estocagem | ASTM D 6930/19 modificado Amostra estocada sedimentação | viscosidade rotacional |
| | | B - 24 horas razão de separação (Rs) (η topo / η fundo) |
| | | C - 24 horas razão de estabilidade η Antes / η Depois condicionamento (Rd) |
| Resistência a cura precoce | AASHTO TP 91-11 BBS | A - mínimo resistência à tração POS |
| | Resistencia a adesão do ligante | XX h de tempo de cura |



NCHRP 09-63 Draft EAPG Specification (V1): Chip Seals

| Emulsion Performance Grade | EPG 55 | | | | | EPG 61 | | | | | EPG 67 | | | |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------|-------|-------|-------|-------|--------|-------|-------|-------|-------|--------|-------|-------|-------|
| | -19 | -25 | -31 | -37 | -43 | -13 | -19 | -25 | -31 | -37 | -13 | -19 | -25 | -31 |
| Surface design high temperature ¹ , °C | < 55 | | | | | < 61 | | | | | < 67 | | | |
| Surface design low temperature ¹ , °C | > -19 | > -25 | > -31 | > -37 | > -43 | > -13 | > -19 | > -25 | > -31 | > -37 | > -13 | > -19 | > -25 | > -31 |
| Tests on Recovered Residue (AASHTO R78, Procedure B) | | | | | | | | | | | | | | |
| High Temperature Parameter | | | | | | | | | | | | | | |
| $G^*/\sin \delta \geq 0.65$ kPa, 10 rad/s @ Test Temperature, °C ² | 55 | | | | | 61 | | | | | 67 | | | |
| Low Temperature Parameter | | | | | | | | | | | | | | |
| G^* at δ_c , MPa ³ | | | | | | | | | | | | | | |
| Low Traffic ⁴ $G^* \leq 30$ MPa @ δ_c , degrees | 48 | 45 | 42 | 39 | 36 | 51 | 48 | 45 | 42 | 39 | 51 | 48 | 45 | 42 |
| High Traffic ⁵ $G^* \leq 15$ MPa @ δ_c , degrees | | | | | | | | | | | | | | |
| OPTIONAL Polymer Presence Indicator | | | | | | | | | | | | | | |
| Max. δ at $T_{c,high}$, degrees ⁶ | n/a | n/a | n/a | 84 | 80 | n/a | n/a | n/a | 84 | 80 | n/a | n/a | 84 | 80 |
| NOTES: | | | | | | | | | | | | | | |
| 1 Determined at the pavement surface to represent the high and low design temperature for the EPG. Temperatures may be determined from experience or may be estimated using equations LTPPBind Online, modified to represent the expected surface temperature. High surface temperatures are generally 3°C to 4°C greater than those determined for PG asphalt binders used for paving. | | | | | | | | | | | | | | |
| 2 AASHTO T315 is used to determine the $G^*/\sin \delta$ value of the EPG asphalt binder. | | | | | | | | | | | | | | |
| 3 G^* at δ_c is determined using temperature-frequency sweep testing at 5 and 15°C following the research test procedure described in NCHRP Report 837. | | | | | | | | | | | | | | |
| 4 Low traffic is defined as having an AADT of 1,000 vehicles or less. | | | | | | | | | | | | | | |
| 5 High traffic is defined as having an AADT greater than 1,000 but less than 20,000 vehicles. | | | | | | | | | | | | | | |
| 6 Phase angle (δ) is determined at the continuous high temperature grade – $T_{c,high}$ – where $G^*/\sin \delta = 0.65$ kPa. Two temperatures are needed – one where $G^*/\sin \delta < 0.65$ kPa and one where $G^*/\sin \delta > 0.65$ kPa – so that the phase angle can be interpolated at the temperature where $G^*/\sin \delta = 0.65$ kPa. | | | | | | | | | | | | | | |

Obtenção do resíduo da emulsão

J. Mater. Civ. Eng., 2024, 36(10): 04024315

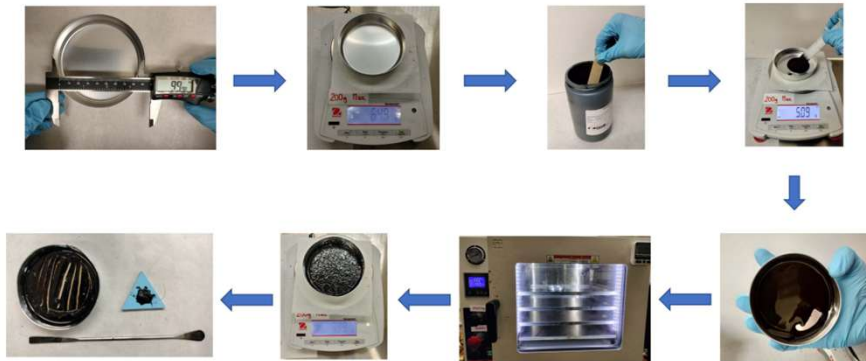
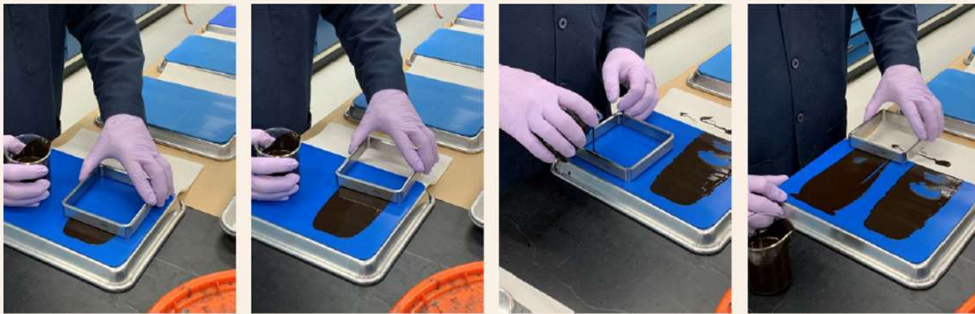


Fig. 2. Step-by-step guide for emulsion residue recovery.

ASTM D7944-15 Standard Practice for Recovery of Emulsified Asphalt Residue Using a Vacuum Oven

Estufa a 70°C e vácuo de 90mBar por 2 horas

AASHTO R 78 Procedure B and ASTM D7944



24 horas a temperatura ambiente seguido por 24 horas em estufa de ar forçada a 60°C

Resistencia a deformação permanente

| | EPG 55 | | | | | EPG 61 | | | | | EPG 67 | | | | |
|-------------------------------------------------------------------|--------|-----|-----|-----|-----|--------|-----|-----|-----|-----|--------|-----|-----|-----|--|
| Grau de desempenho da emulsão | -19 | -25 | -31 | -37 | -43 | -13 | -19 | -25 | -31 | -43 | -13 | -19 | -25 | -31 | |
| Temperatura baixa do pavimento, °C | 55 | | | | | 61 | | | | | 67 | | | | |
| Temperatura alta do pavimento, °C | -19 | -25 | -31 | -37 | -43 | -19 | -25 | -31 | -37 | -43 | -13 | -19 | -25 | -31 | |
| Testes no resíduo da emulsão | | | | | | | | | | | | | | | |
| Ensaio | | | | | | | | | | | | | | | |
| $G^*/\sin\delta > 0,65\text{kPa}$, 10 rad/s na temperatura teste | 55 | | | | | 61 | | | | | 67 | | | | |



Resistencia a trincamento

| Grau de desempenho da emulsão | EPG 55 | | | | | EPG 61 | | | | | EPG 67 | | | |
|------------------------------------|--------|-----|-----|-----|-----|--------|-----|-----|-----|-----|--------|-----|-----|-----|
| | -19 | -25 | -31 | -37 | -43 | -13 | -19 | -25 | -31 | -43 | -13 | -19 | -25 | -31 |
| Temperatura baixa do pavimento, °C | 55 | | | | | 61 | | | | | 67 | | | |
| Temperatura alta do pavimento, °C | -19 | -25 | -31 | -37 | -43 | -19 | -25 | -31 | -37 | -43 | -13 | -19 | -25 | -31 |
| Testes no resíduo da emulsão | | | | | | | | | | | | | | |
| G* a δ_c , MPa | 48 | 45 | 42 | 39 | 36 | 51 | 48 | 45 | 42 | 39 | 51 | 48 | 45 | 42 |
| Baixo tráfego | | | | | | | | | | | | | | |
| G < 30 Mpa a δ_c , ° | | | | | | | | | | | | | | |
| Alto tráfego | | | | | | | | | | | | | | |
| G < 15 Mpa a δ_c , ° | | | | | | | | | | | | | | |



Especificação australiana – parâmetro de resistência a deformação permanente Emulsão modificada 2020

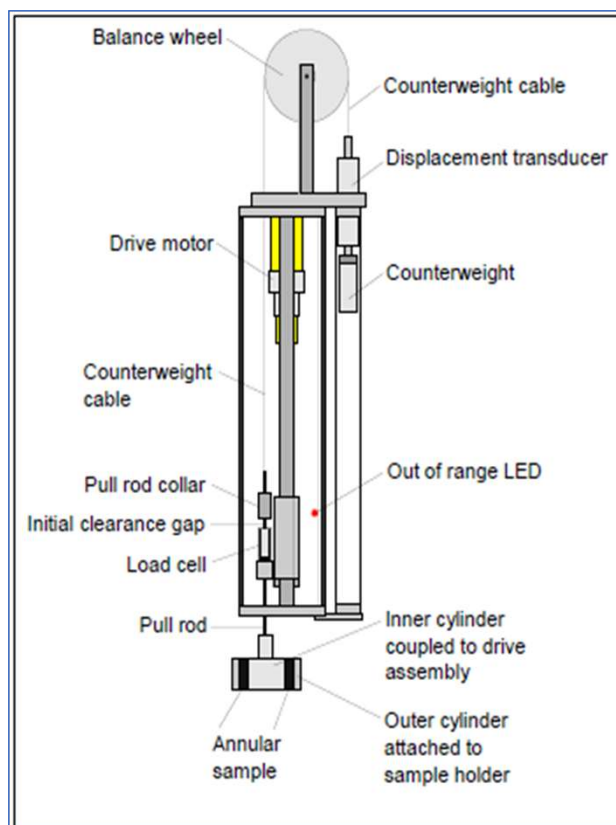


TABLE 511.4 PROPERTIES OF PMB FOR SPRAYED SEALING

| Binder Property | Test Method | Binder Class | | | | |
|------------------------------------------------|--------------------------------|--------------|--------|--------|--------|------------------|
| | | S10E | S20E | S25E | S35E | S45R (Note 2) |
| Stress ratio at 10 °C Minimum | AG:PT/T125 | Report | Report | Report | Report | Report |
| Consistency 6% at 60°C (Pa.s) Minimum | AG:PT/T121 (Note 1) | 300 | 500 | 900 | 250 | 800 |
| Stiffness at 15°C (kPa) Maximum | AG:PT/T121 | 140 | N/A | N/A | 180 | Report |
| Stiffness at 25°C (kPa) Maximum | AG:PT/T121 | N/A | 35 | 30 | N/A | N/A |
| Compressive Limit at 70°C, 2kg mm (minimum) | AG:PT/T132 | N/A | N/A | N/A | N/A | 0.2 |
| Viscosity at 165°C (Pa.s) Maximum (Note 3) | AG:PT/T111 or AS/NZS 2341.4 | 0.55 | 0.6 | 0.9 | 0.55 | 4.5 |
| Flash Point (°C) Minimum | AG:PT/T112 | 250 | 250 | 250 | 250 | 250 |
| Loss on Heating (% mass) Maximum | AG:PT/T103 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |

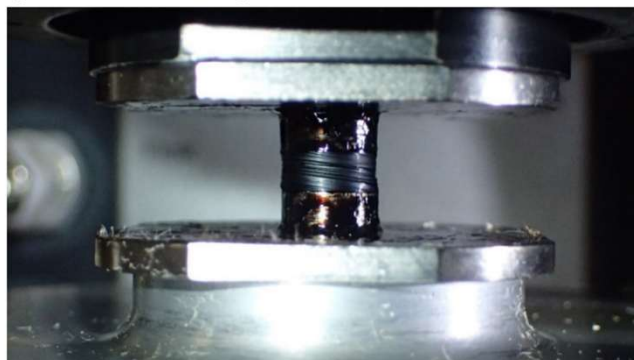
Especificação australiana – parâmetro de resistência a fadiga - taxa de tensão a 10°C
Emulsão modificada 2020

Razão de tensão a 10°C

TABLE 511.4 PROPERTIES OF PMB FOR SPRAYED SEALING

| Binder Property | Test Method | Binder Class | | | | |
|------------------------------------------------|--------------------------------|--------------|--------|--------|--------|------------------|
| | | S10E | S20E | S25E | S35E | S45R (Note 2) |
| Stress ratio at 10 °C Minimum | AG:PT/T125 | Report | Report | Report | Report | Report |
| Consistency 6% at 60°C (Pa.s) Minimum | AG:PT/T121 (Note 1) | 300 | 500 | 900 | 250 | 800 |
| Stiffness at 15°C (kPa) Maximum | AG:PT/T121 | 140 | N/A | N/A | 180 | Report |
| Stiffness at 25°C (kPa) Maximum | AG:PT/T121 | N/A | 35 | 30 | N/A | N/A |
| Compressive Limit at 70°C, 2kg mm (minimum) | AG:PT/T132 | N/A | N/A | N/A | N/A | 0.2 |
| Viscosity at 165°C (Pa.s) Maximum (Note 3) | AG:PT/T111 or AS/NZS 2341.4 | 0.55 | 0.6 | 0.9 | 0.55 | 4.5 |
| Flash Point (°C) Minimum | AG:PT/T112 | 250 | 250 | 250 | 250 | 250 |
| Loss on Heating (% mass) Maximum | AG:PT/T103 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |

Figure 9.1: Distressed binder after testing



Conclusões – Ensaio reológico EPG

- Ensaio de trabalhabilidade devem ajudar na aplicação;
- Ensaio reológico no resíduo da emulsão podem vir a garantir a seleção do ligante de acordo com clima e tráfego;
- Mais testes em campo nos estados americanos irão melhorar ainda mais a escolha dos ensaios e dos limites;
- A concepção da especificação australiana está relacionada apenas ao AMP usado na emulsão, ainda leva em conta alguns ensaios empíricos;



Programa de Engenharia Civil

COPPE - Universidade Federal do Rio de Janeiro

COPPE 60
UFRJ anos

CONCEITO
MÁXIMO 7
CAPES

Obrigada pela atenção !

lenimathias@coc.ufrj.br

Referências

- NCHRP RESEARCH REPORT 837 -Performance-Related Specifications for Emulsified Asphaltic Binders Used in Preservation Surface Treatments (2017)
- Anderson M. -Testing and Specification for Performance-Graded Emulsified Asphalt -AASHTO TSP2 Emulsion Task Force (ETF) Meeting 2019
- Martin, A. et al -Evolution of Performance-Graded Specifications for Chip Seal Binders in the United States- *13th Conference on Asphalt Pavements for southern Africa 2019*
- NCHRP 09-63: A Calibrated and Validated National Performance Related Specification for Emulsified Asphalt Binder
- Gierhart ,D. Innovative Trends in National Asphalt Research SPTC Summer Transportation Symposium 2024
- Anderson, M. Progress Toward the Development of a National Performance-Related Specification for Emulsified Asphalt Binder 2024 AEMA- ARRA –ISSA Annual Meeting
- Schuler et al Guide Specifications for the Construction of Chip Seals, Microsurfacing, and Fog Seals NCHRP 14-37 (2018)
- Anderson, M National Performance-Related Specification for Emulsified Asphalt Binder AASHTO TSP-2 ETF Meeting 2023
- Satyavati et al Evaluation of Using Vacuum Oven for Residue Recovery of Asphalt Emulsion and Cutback Asphalt for Routine Screening J. Mater. Civ. Eng., 2024, 36(10): 04024315
- Mohanraj et al -Field Validation on the Use of Poker-Chip Test to Predict Cracking in Flexible Pavements - J. Transp. Eng., Part B: Pavements, 2023, 149(2): 04023008
- Austroads AUSTROADS TECHNICAL SPECIFICATION ATS3110 Supply of Polymer Modified Binders Edition 1.0 January 2020
- Main Roads Western Australia MATERIALS FOR BITUMINOUS TREATMENTS SPECIFICATION 511 10/4287-002 Issued 06/02/2025
- TxDOT Designation: Tex-554-C Low temperature DYNAMIC SHEAR RHEOMETER testing of asphalt Binder
- Zhou et al - LABORATORY EVALUATION OF ASPHALT BINDER RUTTING, FRACTURE, AND ADHESION TESTS FHWA/TX-14/0-6674-1 april, 2014
- Choi et al - Development of Australian Performance-based Specifications for Bituminous Binders Proceedings of the 2019 World Transport Convention Beijing, China, June 13-16, 2019
- AASHTO T 405 -23 Determination of asphalt binder ductility failure using double edge notched tension DENT
- ASPHALT INSTITUTE (2019). Use of the Delta Tc parameter to characterize asphalt binder behavior. IS240. Asphalt Institute Technical Advisory Committee.
- CHRISTENSEN, D.W.; TRAM, N. (2022). Relationships between the fatigue properties of asphalt binders and the fatigue performance of asphalt mixtures. NCHRP PROJECT 09-59.
- ANDERSON, R.M. et al. (2011). Evaluation of the relationship between asphalt binder properties and non-load related cracking. Association of Asphalt Paving Technologists, v.80, p.615-663.
- ALISOV, A. et al. (2018). A novel method to characterize asphalt binder at high temperature. Road Materials and Pavement Design, v.21, n.1, p.143-155.
- GONZÁLEZ, M. et al. (2018). Reología de los ligantes españoles en el contexto del anexo informativo de la nueva EN12591. XIII Jornada Nacional - ASEFMA 2018.